PHILLIPS MTN VIEW A1 STATE 796
SW NE 10-17S-15E PIMA CO.

COUNTY PIMA AREA 14 mi.SE of Tucson LEASE NO. State 51389

WELL NAME PHILLIPS PETROLEUM MTN VIEW A1 STATE (Strat test)

LOCATION SW NE SEC 10 TWP 17S RANGE 15E FOOTAGE 2630 FNL, 1860 FEL

ELEV ~~3086 est.~~ 3141 GR _____ KB _____ SPUD DATE 6-6-82 STATUS P+A 7-22-82 COMP. DATE 7-22-82 Comp. rept 3-1-83 TOTAL DEPTH 8333

CONTRACTOR Loffland Brothers Co., P.O. Box 3565, Grand Junction, CO 81501

CASING SIZE	DEPTH	CEMENT	LINER SIZE & DEPTH

DRILLED BY ROTARY _____
DRILLED BY CABLE TOOL _____
PRODUCTIVE RESERVOIR _____
INITIAL PRODUCTION _____

FORMATION TOPS	DEPTHS	SOURCE L.L.	SOURCE E.L.	REMARKS

ELECTRIC LOGS	PERFORATED INTERVALS	PROD. INTERVALS
BHC-Sonic Log 1082'	Comp Neut. Fm Den. 8327'	
Dual Induct-SFL	Dipmeter - 8315'	
BHC-Sonic Log 8315'	Sidewall Core Samples 8327'	
Dual Induct 8315'	Mud Log 47'-8333'	

SAMPLE LOG _____
SAMPLE DESCRP. _____
SAMPLE NO. 1840
CORE ANALYSIS _____
DSTs _____

REMARKS _____

APP. TO PLUG _____
PLUGGING REP. _____
COMP. REPORT _____

WATER WELL ACCEPTED BY _____

BOND CO. SAFECO Ins. Co. of Amer.(Filed P/N 702) BOND NO. 41 00 519 DATE 9-20-80

BOND AMT. $ 25,000 CANCELLED 8-27-87 ORGANIZATION REPORT x

FILING RECEIPT 2217 LOC. PLAT x WELL BOOK x PLAT BOOK x

API NO. 02-019-20015 DATE ISSUED 2-1-82 DEDICATION _____

PERMIT NUMBER 796

CONFIDENTIAL

(over)

Release Date _____

RECEIVED

MAR 3 1983

O & G CONS. COMM.

WELL COMPLETION OR RECOMPLETION REPORT AND WELL LOG

DESIGNATE TYPE OF COMPLETION:

New Well [X] Work-Over [ ] Deepen [ ] Plug Back [ ] Same Reservoir [ ] Different Reservoir [ ] Oil [ ] Gas [ ] Dry [X]

DESCRIPTION OF WELL AND LEASE

Operator: Phillips Petroleum Company	Address: P.O. Box 2920, Casper, WY 82602
Federal, State or Indian Lease Number or name of lessor if fee lease: Mountain View State-A (Lse #51389)	Well Number: 1
Field & Reservoir: Wildcat	
Location: 2630' FNL & 1860' FEL, SW NE (1)	County: Pima
Sec. TWP-Range or Block & Survey: Sec. 10-T17S-R15E	

Date spudded	Date total depth reached	Date completed, ready to produce	Elevation (DF, RKB, RT or Gr.) feet	Elevation of casing hd. flange feet
6/6/82	7/21/82	P&A 7/22/82	GR 3141'	--

Total depth	P.B.T.D.	Single, dual or triple completion?	If this is a dual or triple completion, furnish separate report for each completion.
8333'	--	--	--

Producing interval (s) for this completion	Rotary tools used (interval)	Cable tools used (interval)
--	0 - 8333'	--

Was this well directionally drilled?	Was directional survey made?	Was copy of directional survey filed?	Date filed
No	No	--	--

Type of electrical or other logs run (check logs filed with the commission)	Date filed
DIL-SP-GR, BHC-Sonic-CAL	Approx. 6/14/82

CASING RECORD

Casing (report all strings set in well—conductor, surface, intermediate, producing, etc.)

Purpose	Size hole drilled	Size casing set	Weight (lb./ft.)	Depth set	Sacks cement	Amt. pulled
Surface	12-2/4"	9-5/8"	40#	1071'	913 sx Class G	--

TUBING RECORD

Size	Depth set	Packer set at
-- in.	-- ft.	-- ft.

LINER RECORD

Size	Top	Bottom	Sacks cement	Screen (ft.)
-- in.	-- ft.	-- ft.	--	--

PERFORATION RECORD

Number per ft.	Size & type	Depth Interval
--	--	--

ACID, SHOT, FRACTURE, CEMENT SQUEEZE RECORD

Am't. & kind of material used	Depth Interval
Set 130 sx Type G cmt	plug 1175-980'.
Set 10 sx cmt plug at	surface.

INITIAL PRODUCTION

Date of first production: --

Producing method (indicate if flowing, gas lift or pumping—if pumping, show size & type of pump:): Plugged & Abandoned 7/22/82

Date of test	Hrs. tested	Choke size	Oil prod. during test	Gas prod. during test	Water prod. during test	Oil gravity
--	--	--	-- bbls.	-- MCF	-- bbls.	-- ° API (Corr)

Tubing pressure	Casing pressure	Cal'ted rate of Production per 24 hrs.	Oil	Gas	Water	Gas—oil ratio
--	--		-- bbls.	-- MCF	-- bbls.	--

Disposition of gas (state whether vented, used for fuel or sold): --

CERTIFICATE: I, the undersigned, under the penalty of perjury, state that I am the Area Manager of the Phillips Petroleum Company (company), and that I am authorized by said company to make this report; and that this report was prepared under my supervision and direction and that the facts stated therein are true, correct and complete to the best of my knowledge.

Date 3/1/83

Signature D. J. Fisher

1 - State of Arizone
1 - B'Ville
1 - Denver
1 - File

Permit No. 796

STATE OF ARIZONA
OIL & GAS CONSERVATION COMMISSION
Well Completion or Recompletion Report and Well Log
File One Copy
Form No. 4

(Complete Reverse Side)

DETAIL OF FORMATIONS PENETRATED

Formation	Top	Bottom	Description*
CORES			
8325' - 8333' -- Cored 8', Rec 7.4'			
Ran sidewall cores from 5630-7170', 48 shots, 14 sidewall cores rec.			
NO DST'S			
NO POROSITY			
			Phillips Petroleum Mountain View A-1 State; Section 10, T.17 S., R.15 E., Pima County. T. D. at 8333 feet in Tertiary granite dated at 16.7 M. Y. with K-Ar.

* Show all important zones of porosity, detail of all cores, and all drill-stem tests, including depth interval tested, cushion used, time tool open, flowing and shut-in pressures, and recoveries.

INSTRUCTIONS:

Attach drillers log or other acceptable log of well.

This Well Completion or Recompletion report and well log shall be filed with the State of Arizona Oil & Gas Conservation Commission not later than thirty days after project completion.

Form No. 4

RECEIVED
MAR 7 1983
OIL & GAS CONS. COMM.

PLUGGING RECORD

Operator: Phillips Petroleum Company	Address: P.O. Box 2920, Casper, WY 82602
Federal, State, or Indian Lease Number, or lessor's name if fee lease: Lse #51389 Mountain View State-A	Well No.: 1
Field & Reservoir: Wildcat	
Location of Well: 2630' FNL & 1860' FEL, SW NE Sec. 10-T17S-R15E	Sec-Twp-Rge or Block & Survey
County: Pima	
Application to drill this well was filed in name of: Phillips Petroleum Company	Has this well ever produced oil or gas: No
Character of well at completion (initial production): Oil (bbls/day): 0	Gas (MCF/day): 0
Dry?: Yes	
Date plugged: 7/22/82	Total depth: 8333'
Amount well producing when plugged: Oil (bbls/day): 0	Gas (MCF/day): 0
Water (bbls/day): 0	

Name of each formation containing oil or gas. Indicate which formation open to wellbore at time of plugging	Fluid content of each formation	Depth interval of each formation	Size, kind & depth of plugs used. Indicate zones squeeze cemented, giving amount cement
None	None	---	Set 130 sx Type G cmt plug 1175-980'. Set 10 sx cmt plug at surface.

CASING RECORD

Size pipe	Put in well (ft.)	Pulled out (ft.)	Left in well (ft.)	Give depth and method of parting casing (shot, ripped, etc.)	Packers and shoes
9-5/8"	1071'	--	1071'	No Recovery	Shoe at 1071'

Was well filled with mud-laden fluid, according to regulations? Yes

Indicate deepest formation containing fresh water. NA

NAMES AND ADDRESSES OF ADJACENT LEASE OPERATORS OR OWNERS OF THE SURFACE

Name	Address	Direction from this well:
Information not available to this office.		

In addition to other information required on this form, if this well was plugged back for use as a fresh water well, give all pertinent details of plugging operations to base of fresh water sand, perforated interval to fresh water sand, name and address of surface owner, and attach letter from surface owner authorizing completion of this well as a water well and agreeing to assume full liability for any subsequent plugging which might be required.

NA

Use reverse side for additional detail.

CERTIFICATE: I, the undersigned, under the penalty of perjury, state that I am the Area Manager of the Phillips Petroleum Company (company) and that I am authorized by said company to make this report; and that this report was prepared under my supervision and direction and that the facts stated therein are true, correct and complete to the best of my knowledge.

Date: 3/3/83

Signature: D. J. Fisher

X - State of Arizona
1 - B'Ville
1 - Denver
1 - File

Permit No. 796

STATE OF ARIZONA
OIL & GAS CONSERVATION COMMISSION
Plugging Record
File One Copy

Form No. 10

Drilling & Casing Program:

Drill 12-1/4" hole to 1000' . Set 9-5/8" and TD with 7-7/8" hole. Set 1 jt. of 14" conductor; drill 12-1/4" hole, to firm casing seat at approximately 1000'. Run 9-5/8" 40# K-55 ST&C Casing (3759 psi Burst, 2487 psi Collapse, 324,000# Tensile. 4860 ft-lbs optimum torque w/3650 ft-lbs minimum & 6080 ft-lbs. maximum torque). Run one centralizer directly above the shoe, another on the second joint, another approximately 150' above the shoe and then every 200 ' to the surface. Use Philube API modified thread lubricant, circulate casing volume of 76 bbls. Preflush with 20 bbls. fresh water spacer followed by 250 sx Cl. "G" w/10% Diacel "D" w/2% Gel (Yield 2.09 CF/sx, Mix @ 12.8 ppg) followed by 100 sx Cl. "G" neat as tail-in (yield 1.15 CF/sx, mix @ 15.8 ppg) Above volumes are on a design basis of 100% above theoretical for a 9-5/8" x 12-1/4" annulus, or equivalent to a 14-3/8"avg. hole diameter. Adjust, if necessary to the 10% Diacel "D" volume. Run standard Super Seal Float Collar and Float Shoe. Howco in El Centro has FC&FS and 8 centralizers and will bring to location. WOC 18 hrs. before commencing to nipple-up.

Drilling Mud-Program attached. To be supplied by Baroid under Farmington, New Mexico Office. District Manager of Baroid is Bob Hogg, Farmington (505) 325-1896 (o) and (505) 325-5486 (r). Local contacts are Bill Harder, Tucson, (602) 885-8910; Tim Adams Solar City, New Mexico (505) 388-3315; Dennis Woods, Sr. Engr. Phoenix, (602) 963-8069.

Mobils:	Dennis Woods	(0414) (602) 253-6143
	Bill Harder	(0110) (602) 624-6646
	Tim Adams	(2445) (505) 538-5376

Mobils are not direct dial; Woods and Harders are with General Communications; Adams is with Sierra Communications; numbers in parenthesis refer to unit or vechicle radios numbers with these services.

BOP's-Nipple up after setting 9-5/8" per BOP Standard Figure 6 or 7 (depending upon rig equipment). Test BOP's initially and first trip out-of-hole after Tuesday, A.M. With 1000' of casing, test pressure need not exceed 1500 psig.

Mud Logging Unit - Continental Laboratories will furnish hydrocarbon well logging services and Exploration has contracted. Contact is Continental Labs, Denver, Colorado, Steve Leibbrand (303) 751-0101.

Well Head - Three 9-5/8" S.O. x 10" Series 900 Braden Heads w/3 R53 Ring Gaskets and 2 boxes of nuts and bolts were purchased from National Supply, Farmington, (505) 325-1723 and hauled to Baroids Tucson yard with a load of mud from Baroid in Farmington.

Formation Tops

Quaternary	Spud
Base of Tertiary/Top of Cretaceous/Paleozic	2200'
Trust fault	6000'
T.D.	9000'

Objective Horizons

Primary objective is to test horizons interpreted from seismic reflectors to be Paleozoic in age. Objectives within the Cretaceous include the Apache Canyon Formation and within the Paleozoic, the Pennsylvanian Horquilla Limestone.

Logging Program

Run No. 1

12 1/4" Hole Surface to 1000' or deeper (9-5/8" csg. pt.)

1. DIL-SP-BHC Sonic-GR
If hole is deeper than 1,000', also run;
2. FDC-CNL-GR Caliper
3. HDT

Run No. 2

7-7/8" Hole 9-5/8" csg. depth-T.D.

1. DIL-SP-BHC Sonic-GR
2. FDC-CNL-GR Caliper
3. HDT

All electric logs will be taped; distribution of logs will be by Exploration. Two sets of maximum reading thermometers, three per set, in the ranges of 100 deg.-300 deg. F. will be available for use on all logging runs. Thermometers should have been recently calibrated.

Coring Program

At the direction of the Phillips' Wellsite Geologist cores or sidewall cores will be taken in intervals of stratigraphic interest, intervals exhibiting significant hydrocarbon shows and/or at T.D.

Cores will be measured, marked and clearly labelled prior to being packed in boxes. A sheet of paper bearing the well name, core number and interval will be inserted in a plastic sample sack and packed within each box prior to securing the lid. Each box will be labelled on either end with well name, core number and interval.

Sample Program

Sample catching at 10 feet intervals, will commence at the surface or as soon thereafter as is practicable and will be continued to T.D.

Detailed instructions and requirements covering the number of sets required, sample treatment, handling, packaging, and shipping instructions will be covered in a separate memorandum.

Geological Well Prognosis
for
PPCO. MOUNTAIN VIEW STATE NO. 1

A. Lithologies Expected to be Encountered

The well is expected to spud in Precambrian granite and penetrate approximately 1000 feet of crystalline rock. The next section from 1000 ft. to T.D. (9000 ft.) is interpreted to be Paleozoic in age. The Paleozoic rocks are composed of a wide variety of sedimentary strata including both carbonates and clastics ranging from shales and mudstones to sandstones. It is possible that some or all of the lithology in this section is composed of Precambrian crystalline rock including metasediments and metavolcanics (schists and amphibolities), and granite.

B. Potential Drilling Program

Lost circulation could possibly occur within fractured Precambrian crystalline rocks and within porous Paleozic sedimentary rocks. Since at least two major thrust faults are expected to be encountered, lost circulation might occur within these fault zones. Also steep dips might be encountered while crossing these thrust faults which would cause deviation problems.

Recommended Mud Program

The mud should have sufficient viscosity and low water loss to insure good samples and ingauge hole conditions for the log runs throughout the drilling of this well.

At the present time in this very sparsely drilled area, we are unaware of any abnormally pressured zones. We, therefore, anticipate normally pressured (.433# per foot) reservoir pressures to total depth.

Well Log Info. Distribution List:

Algonquin Gas & Transmission Co.
1284 Soldiers Field Road
Boston, Mass. 02135
Attn: Mr. Terry Ray

The Anschutz Corp
555 17th Street
Denver, CO 80202

Anthrust Inc.
P.O. Box 5928
Denver, CO 80217
Attn: Mr. Al Sanborn
303-825-4771

Connecticut Mutual Life
140 Garden Street
Hartford, Connecticut 06115
Attn: Mr. Ken Anderson

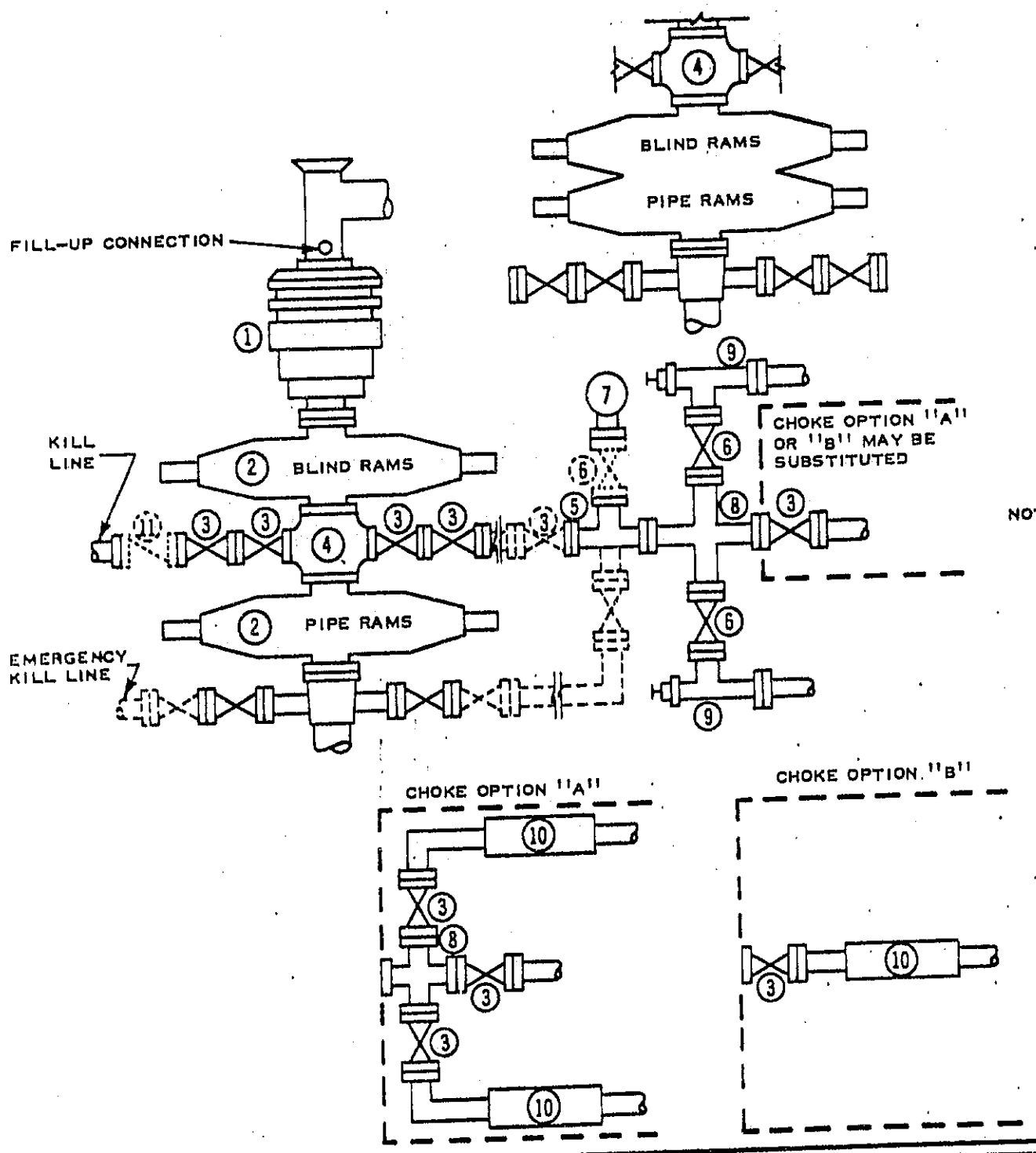
Huron Petroleum Corp.
410 17th Street, Suite 2300
Denver, CO 80202
Attn: Mr. Robert Magnie 303-825-1966

Merrill Evans
Phillips Petroleum Co. Denver, CO
303-779-8989, Ext. 608

FGL/fb
Attach.

cc: D. J. Fisher
P. B. Hammaker
F. G. Lyte(3)
J. L. Sanford
Norm Johnson (2)

DOUBLE PREVENTER OPTION



1. SER. 900 HYDRIL "GK"
2. SER. 900 RAM-TYPE BOP
3. 3" SER. 900 VALVE
4. SER. 900 DRILLING SPOOL
5. 3" SER. 900 X 2" SER. 900 STEEL TEE
6. 2" SER. 900 VALVE
7. 2" MUD PRESSURE GAUGE
8. 3" SER. 900 X 2" SER. 900 STEEL CROSS
9. 2" SER. 900 ADJ. CHOKE
10. HYDRAULIC CHOKE, 2500 PSI WP OR BETTER
11. 3" SER. 900 CHECK VALVE

NOTES:

1. 3000 PSI WP OR BETTER CLAMP HUBS MAY BE SUBSTITUTED FOR FLANGES
2. ONE ADJUSTABLE CHOKE MAY BE REPLACED WITH A POSITIVE CHOKE
3. VALVES MAY BE EITHER HAND OR POWER OPERATED BUT, IF POWER OPERATED, THE VALVES FLANGED TO THE BOP RUN MUST BE CAPABLE OF BEING OPENED AND CLOSED MANUALLY OR CLOSE ON POWER FAILURE AND BE CAPABLE OF BEING OPENED MANUALLY

..... OPTIONAL EQUIPMENT

PHILLIPS PETROLEUM COMPANY

3000 PSI WORKING PRESSURE

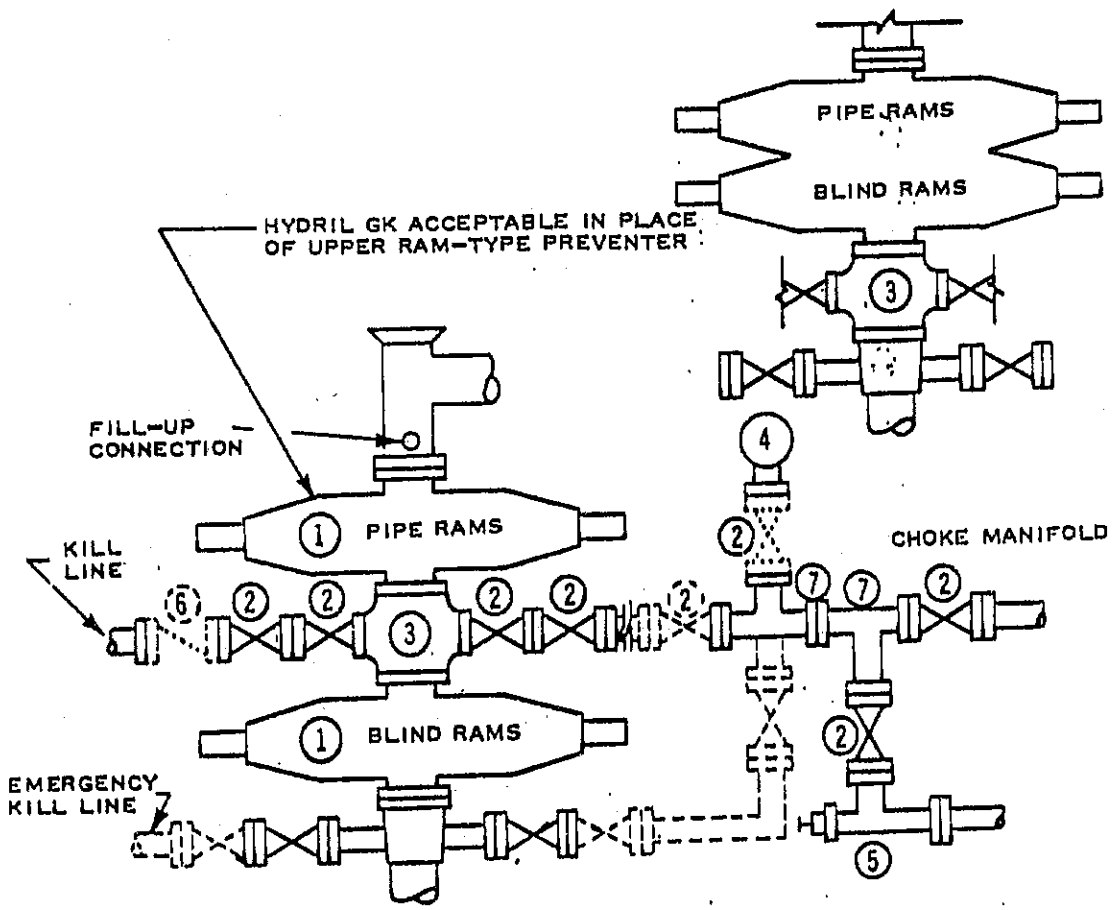
BLOWOUT PREVENTER HOOK-UP

(SERIES 900 FLANGES OR BETTER)

REV 6/73

FIGURE NO. 6

DOUBLE PREVENTER OPTION



1. SERIES 900 RAM-TYPE BOP
2. 2" SERIES 900 VALVE
3. SERIES 900 DRILLING SPOOL
4. 2" MUD PRESSURE GAUGE
5. 2" SERIES 900 CHOKE
6. 2" SERIES 900 CHECK VALVE
7. 2" SERIES 900 STEEL TEE

NOTES:

1. 3000 PSI WP CLAMP HUBS MAY BE SUBSTITUTED FOR FLANGES
2. VALVES MAY BE EITHER HAND OR POWER OPERATED BUT, IF POWER OPERATED, THE VALVES FLANGED TO THE BOP RUN MUST BE CAPABLE OF BEING OPENED AND CLOSED MANUALLY OR CLOSE ON POWER FAILURE AND BE CAPABLE OF BEING OPENED MANUALLY

..... OPTIONAL EQUIPMENT

PHILLIPS PETROLEUM COMPANY

3000 PSI WORKING PRESSURE BLOWOUT PREVENTER HOOK-UP

(SERIES 900 FLANGES OR BETTER)

REV 6/73

FIGURE NO. 7

PHILLIPS PETROLEUM COMPANY

ARIZONA STRAT WELLS

HOLE SIZE AND CASING PROGRAM:

Hole Size	Casing Size	Depth
12-1/4"	9-5/8"	1000'-2000'±
7-7/8"	-	T.D.

INTERVAL	MUD TREATMENT AND PROPERTIES
0-9-5/8" C.P.	Spud Mud. Mix 10.0 lbs/bbl, Bentonite 15 lbs/bbl. Diacel® diatomateous solids, 3 to 5 lbs/bbl fibrous type LCM. This mixture of materials will produce a fluid that will clean the hole efficiently, minimize hole enlargement and treat all but very major mud losses as they are drilled. Use the above ratio of materials to maintain and/or rebuild volume as needed.
9-5/8" C.P.-T.D.	(1.) Drill out of surface casing with water and discard cement contaminated fluid.
	(2.) In clean, fresh water - mix caustic soda to obtain 9.5 to 10.5 pH.
	(3.) Mix sack ratio of 8 sks. bentonite to 1 sk. Drispac® polymer to build funnel voscosity of 34 to 38 sec/qt.
	(4.) Stay on this (8:1) bentonite/Drispac ratio at all times to maintain viscosity. This ratio will produce a low solids drilling fluid that will automatically have a controlled water loss w/good thin, slick filter cake that should keep the hole in good shape for logging, coring, and D.S.T.'s. This fluid should bring up clean, large cuttings which will aid geological evaluation of formations drilled.
	(5.) Drilling water supply is likely to be a major cost item on this well. Therefore, a semi-closed mechanical solids control system should be utilized. (A.) High speed, fine screen shale shakers (using finest screens feasible), (B.) Desander and mud cleaner or desilter units that will each handle 50% more volume than that being circulated. (C.) A high speed - high volume centrifuge to discard maximum low gravity drilled solids, will also be considered.

(6.) Maintain Mud:

Weight – 8.6 to 9.2 #/gal or minimum needed to maintain good hole conditions w/mech. solids control equipment and water.

Viscosity – 36 to 42 sec/qt. w/8:1 Bentonite & Drispac ratio. Stay on this ratio at all times. 45 to 50 sec/qt. to log, DST or core.

Water Loss – 10.0 to 5.0 cc w/additional Drispac as needed above that used for vis. ratio.

pH – 9.5 to 10.5 w/caustic soda.

Total Hardness – Below 300 PPM w/soda ash.

Rheology – Run non-dispersed if possible. Control gel strengths with sack ratio of 1 sk. Desco® thiner to 2 sks lignite, only if needed. Use sparingly.

Loss of Circulation – Do not carry LCM in mud, unless absolutely necessary, in order to be able to utilize all mech. solids control equipment.

A. If extra pit is available: Mix in water – 3 lbs/bbl Ground Paper, 1/2 sk/bbl Diacel D® and 5 lbs/bbl Med. Qwik-Seal (wait to mix Qwik-Seal until loss occurs). When loss is detected while drilling – pull up off bottom, spot above slurry (25 to 50 bbl) in bottom of hole and pull enough drill pipe to get above slurry. 1) Wait 30 minutes; if hole will fill, close hydril and pump into annulus at 1 ± bbl/min until pressure build-up is noticed (100± psi) on drill pipe, watch for bleed-off and repeat until 20± bbls mud has been pumped or holding pressure build-up can be achieved. After above volume is pumped and hole will stand full, wait 30 minutes, break circulation, go back to bottom and drill, 2) If hole will not fill after spotting above slurry, spot another like slurry volume.

B. On serious, complete and sustained losses, the attached Diaseal M® squeeze procedure will be used. NOTE: Substitute Ground Paper when Flosal is not to be used).

NOTES: (1.) Mud materials and service will be supplied by N/L Baroid Mud Co.

(2.) Any significant changes in the program or mud products used must be cleared through the Phillips Casper District Office (307-237-3791) and notification of same to Glen Slater (303) 779-8989 Ext. 384.

(3.) Daily mud check sheets must include total daily mud cost, each material used w/cost and cumulative cost. Also report on-location inventory of mud materials if this is not already a pert of mud check form.

(4.) Once each week mail legible copies of mud check sheets to PPCo., Glen I. Slater, 7800 E. Eldorado Place Room 245, Englewood, CO 80111.

(5.) Submit well recap and mud cost summary to Casper Office and Glen Slater upon completion of well.

cc: D. J. Fisher
P. B. Hammaker
F. G. Lyte
Dist. & Reg. Files
Glen I. Slater (2) Phillips Petroleum Co., 7800 East Dorado Place, Room 245, Englewood, CO 80111

Brinkerhoff-Signal Drilling Co. (2)

N/L Baroid Mud Co. (2)

E. E. Clear, (1) Drlg. Spec. Co., 309 Short St., B'Ville, OK 74004

GENERAL PROCEDURE FOR USING UNWEIGHTED DIASEAL M® OR "MODIFIED" DIACEL D® SLURRY

1) Pull drill string above loss zone or a considered safe distance off bottom when starting to mix the HWL-HS slurry.

2) Put kelly back on--continue to work pipe if in open hole.

3) Mix Diaseal M® or "Modified" Diacel D® slurry--at least 100 bbls. See attached sheet for guide to materials needed and mixing procedures.

4) Mix LCM--continue to work pipe while mixing.

5) Pump mixture in hole and displace drill pipe with mud.

6) Pull up into surface casing or a safe distance above where slurry would fill hole considering no loss to formation. Fill hole through fill-up line.

7) If hole does not fill after pumping about one foot of mud out of pits, mix another slurry volume and repeat procedure. On severe losses when slurry w/normal amounts of LCM is not adequate to seal loss, consider going in hole with open-end drill pipe and pumping out pieces of burlap bags. Cut bags (across bag) into four pieces, soak in mud, roll and drop into drill pipe at surface. Drop 100 quarters then displace out of drill pipe with mud. Follow with another 100 bbl Diaseal slurry (Step 5) and continue squeeze procedure.

8) If hole stands full or has circulated some during Step 5, proceed as follows:

   Close pipe rams or Hydril, pump very slowly through fill-up line at 0-300 psi and squeeze. When pressure starts to build or is indicated while pumping, hesitate (watch for pressure bleed-back) then pump again until a low holding pressure can be established--somewhere between 50 and 300 psi. Hold available pressure for 20-45 minutes. When a squeeze pressure cannot be established wait about 2 hours, then if hole will stand full and circulate with drill string in upper position, go back to bottom and drill.

A low squeeze pressure is highly desirable because incipient fractures in the fractured loss zones will often be opened and plugged immediately, thus reinforcing the zone and decreasing the chance of loss or avoiding later losses. To be most effective, as much of the loss zone as possible should be penetrated before applying this squeeze technique.

Getting a successful squeeze depends entirely upon the high water loss/high solids slurry being placed in the hole so that it will go into the zone of loss. If the loss zone(s) is suspected to be back up the hole rather than at or near bottom, then consideration should be given to running some type tool to locate the zone(s) taking mud.

PROCEDURE FOR MIXING A DIASEAL M® HWL-HS SQUEEZE SLURRY

I. Gun in 100 bags of Diaseal M in 87 bbls water.

II. Gun in ±1,000 lbs fibrous type LCM and the finished 100 bbl of squeeze slurry is ready to pump.

III. If there is very much bentonite or clays left in pit to be used, a few sacks of lime mixed ahead of the other material would insure a high water loss slurry.

IV. If pre-mix or pill pit is available Diacel M® could be mixed and on stand-by. Then when needed, the LCM could be gunned in and slurry would be ready for displacement.

PROCEDURE FOR MIXING A "MODIFIED" DIACEL D® HWL-HS SQUEEZE SLURRY

I. Materials needed for 100 bbls of unweighted slurry:

Water	-	87 bbls
Lime	-	1 (50#) bag
Flosal®	-	6 (50#) bags (or Ground Paper)
Diacel D®	-	100 (50#) bags
LCM	-	±1,000 lbs (±10 lbs/bbl) Fibrous and/or granular type

II. Order of mixing:

1) In ±50 bbls water mix 1 sk lime and 6 sks Flosal®. Gun good with maximum pressure on mud guns in order to mix and shear Flosal®.

2) When Flosal® is mixed well, continue to gun pit while adding remainder of water. Dump the 100 sks of Diacel D® directly into pit under mud guns.

3) Then dump in LCM under mud guns and mix thoroughly.

III. If pre-mix or pill pit is available, the lime, Flosal® and Diacel D® could be mixed and on stand-by. Then when needed, the LCM could be gunned in and slurry would be ready for displacement.

IV. If Flosal® viscosifier cannot be used, simply add extra Diacel D® (as much as ±80 ppb) to obtain thickness desired or needed for adequate suspending ability for LCM or Barite. Extra Diacel D® will help make a better slurry.

NOTE: The Diaseal M® or Diacel D® slurries may be mixed with whatever type water is in use in mud. If oil mud is in use, then make-up oil can be used to compound slurry; however, this should be pilot tested.

GIS:jg 12/11/81

GENERAL PROCEDURE FOR USING WEIGHTED DIASEAL M® OR "MODIFIED" DIACEL D® SLURRY

1) Mix slurry according to attached tables, adding Diacel M® or Diacel D®, Barite and LCM in order. If this is an oil slurry, a minute amount of oil wetting agent will be needed to lower viscosity as Barite (water wet particle) is added. A separate mixing or blending pit is advisable as well as a pump truck to handle and accurately place weighted slurries.

2) Place bottom of drill pipe far enough up into casing (or a safe distance above loss zone if in long open hole section and impractical to be in casing) to displace all of slurry into open hole and bottom of casing. Do not squeeze through bit openings less than 16/32" diameter with LCM in slurry. Open end squeeze is desirable.

3) Pick up slurry with pump truck and displace it out of drill pipe with mud. If up in casing when slurry starts out of drill pipe, close B.O.P.'s making sure annulus is full. If RTT's tool is used, it should be set. Either action prevents migration. When slurry hits open hole, slow pump down to 1/2 to 3/4 bbl/min. If in long open hole section, displace and lay slurry just as laying a cement plug. Pull well above displaced slurry or up into casing before closing BOP's on full annulus.

4) Stage slurry into formation, a few barrels at a time, pumping at rate of 1/4 bbl/min, hesitating for several minutes. Continue this cycle until pressure begins to build with probable pressure build-ups and bleed-offs. A final holding pressure of 300-900 psi is desirable.

5) Hold pressure for two hours before releasing and resume drilling operations.

6) a. Where break-down and loss of circulation is a reasonable distance below a casing shoe, run a slurry volume equal to twice open hole volume.

   b. Where loss is on bottom with long open hole section open, run at least 100 bbl slurry volume.

7) Slurry remaining in hole after squeeze will not contaminate the mud system nor will it set-up like cement. As mud is circulated past a Diaseal M® plug within the formation, the low permeability mud cake will form a final seal over the plug.

FORMULA FOR PREPARING ONE BARREL DIASEAL M® OR MODIFIED DIACEL D® SLURRY WITH FRESH OR SEA WATER*

Density Lb/Gal.	Diaseal M® Lb.	Diaseal M® Sack	Barite* Sack	Water Bbl.
9	50	1.00	0	.87
10	50	1.00	0.6	.84
11	47	.94	1.2	.80
12	42	.84	1.8	.77
13	39	.76	2.3	.74
14	35	.68	2.9	.70
15	31	.62	3.5	.67
16	28	.56	4.0	.63
17	25	.50	4.6	.60
18	22	.44	5.2	.56
19	17	.34	5.8	.52

*If saturated salt water is used, Barite must be decreased 0.6 sack per barrel.

FORMULA FOR PREPARING DIASEAL M® SLURRY WITH OIL*

FOR 100 BBL. OF SLURRY

Density Lb/Gal.	Diaseal M® Sacks	Barite Sacks	Oil Bbl.
8	88	38	88.0
9	82	88	85.5
10	76	138	83.0
11	70	188	80.5
12	65	238	77.0
13	60	290	74.5
14	54	343	72.0
15	48	397	69.5
16	43	452	67.0
17	38	508	64.5
18	33	565	61.0

*Because of variations of oil and Barite, pilot tests should be made to determine exact formulations. If slurry becomes too thick, add up to 1 lb/bbl oil wetting agent to thin.

---

25 lb/bbl of nut shells can be used in above formulations without change. If absorbent lost circulation materials are added, the slurry viscosity will increase. This slurry is effective without conventional lost circulation materials.

GIS:jg 12/11/81

10-25-82 departed for Mtn View well (796)

- Arrived @ 10:00 am + noted:
  1. well monumented
  2. Surf. regraded
  3. the reseeding was not too good — only sporadic clumps thru-out — this prob. because of lack of rain
  4. the undisturbed areas around the well site did not show any grass at all
  5. some cactus is begining to grow thru out graded area

Arrived in Phx @ 3:50 pm + washed car

600 + miles

Drlg Contractor - Joe Salazar
Drlg, Inc.

RECEIVED
JUL 26 1982
O & G CONS. COMM.

SUNDRY NOTICES AND REPORTS ON WELLS

1. Name of Operator Phillips Petroleum Company
2. OIL WELL [X] GAS WELL [ ] OTHER [ ] (Specify)
3. Well Name Mountain View State "A" No. 1
   Location 2630' FNL and 1860' FEL
   Sec. 10 Twp. 17S Rge. 15E County Pima, Arizona.
4. Federal, State or Indian Lease Number, or lessor's name if fee lease State Lease #51389
5. Field or Pool Name Wildcat
6. Check Appropriate Box to Indicate Nature of Notice, Report, or Other Data

NOTICE OF INTENTION TO:				SUBSEQUENT REPORT OF:			
TEST WATER SHUT-OFF	[ ]	PULL OR ALTER CASING	[ ]	WATER SHUT-OFF	[ ]	weekly ~~MONTHLY~~ PROGRESS	[X]
FRACTURE TREAT	[ ]	DIRECTIONAL DRILL	[ ]	FRACTURE TREATMENT	[ ]	REPAIRING WELL	[ ]
SHOOT OR ACIDIZE	[ ]	PERFORATE CASING	[ ]	SHOOTING OR ACIDIZING	[ ]	ALTERING CASING	[ ]
REPAIR WELL	[ ]	CHANGE PLANS	[ ]			ABANDONMENT	[ ]
(OTHER)			[ ]	(OTHER)			[ ]

(NOTE: Report results of multiple completion on Well Completion or Recompletion Report and Log form.)

7. DESCRIBE PROPOSED OR COMPLETED OPERATIONS (Clearly state all pertinent details, and give pertinent dates, including estimated date of starting any proposed work. If well is directionally drilled, give subsurface locations and measured and true vertical depths for all markers and zones pertinent to this work.)

TITE HOLE - CONFIDENTIAL FINAL REPORT

Week of July 17 - July 23, 1982

Tested BOP's, OK to 2000 psi, hydril to 1500 psi. WIH. Drld to 8325', COOH. Surveys - 1-3/4 deg at 7843', 1-1/2 deg at 7935', 2 deg at 8059', 2 deg at 8184'. Mud 9.1, Vis 32, WL 12. RU Schl. to log. Loggers TD 8320'. Ran DILL-SONIC. Malfunction on taping. Ran velocity survey. Reran DILL and SONIC separately. OK. Ran FDC-CNL log. CNL OK, FDC failed. Ran HDT dipmeter. Schlumberger on standby. WIH. Circ. COOH. PU core bbl and WIH. RD Schl. Cut core #1 from 8325' to 8333'. Core jammed. COOH, rec 7.4' of core. Ran sidewall cores from 5630' to 7170', 48 shots, 14 sidewall cores rec. Trip to LDDP. RU Howco, set 130 sx type G cmt plug 1175'-980'. LD 1000' DP. Set 10 sx cmt plug at surface. ND BOP. Clean mud pits. Released rig at 12:00 midnight, 7/22/82. Plugged and abandoned 7/22/82. FINAL REPORT

8. I hereby certify that the foregoing is true and correct.

Signed D. J. Fisher Title Area Manager Date 7/23/82

Permit No. 796

STATE OF ARIZONA
OIL & GAS CONSERVATION COMMISSION
Sundry Notices and Reports On Wells
File One Copy
Form No. 25

7-23-82

Phillips Pet. Mtn View A1 State (796)

7-21-82 Departed Phx @ 3:15 pm (mileage 18,084) 18040
Arrived in Tucson + checked in the La Quinta Motel @ 6:30 pm.
Called Rig several times to get exact schedule on plugging operations - no answer

Drove out to Rig @ 8:00 pm - Johnson had just gotten in + he told that Phillips had decided to take sidewall cores from certain interval, so plugging would be delayed but was not certain how long of a delay - would have a better idea in the morning - went back to Motel.

7-22-82 Went back to Rig + were pulling out w/ coring tool - plugging would be ± 1:30 pm.
@ 2:30 pm. well was plugged from 1180-965'± + from 30'-5' (cellar floor), with 130 Sx + 10 Sx of cement, respectively. T.D. 8333' (cored to 8325')

Departed Rig @ 4:45 pm. + arrived home @ 7:20 pm.

Comment: Reserve pit is empty of all water - it has been sprayed on road for dust control, so as soon as Rig moves out it will be backfilled + the site recontoured - will do own re-seeding of the area w/ a blend of 5 grasses approved by John Beinfor (U. of A.) - should be completed by Wed (July 28)

15 500 (460 miles)

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JUL 19 1982
O & G CONS. COMM.

SUNDRY NOTICES AND REPORTS ON WELLS

1. Name of Operator Phillips Petroleum Company

2. OIL WELL [X] GAS WELL [ ] OTHER [ ] (Specify)

3. Well Name Mountain View State "A" No. 1

Location 2630' FNL and 1860' FEL

Sec. 10 Twp. 17S Rge. 15E County Pima, Arizona.

4. Federal, State or Indian Lease Number, or lessor's name if fee lease State Lease #51389

5. Field or Pool Name Wildcat

6. Check Appropriate Box to Indicate Nature of Notice, Report, or Other Data

NOTICE OF INTENTION TO:				SUBSEQUENT REPORT OF:			
TEST WATER SHUT-OFF	[ ]	PULL OR ALTER CASING	[ ]	WATER SHUT-OFF	[ ]	~~MONTHLY~~ weekly PROGRESS	[X]
FRACTURE TREAT	[ ]	DIRECTIONAL DRILL	[ ]	FRACTURE TREATMENT	[ ]	REPAIRING WELL	[ ]
SHOOT OR ACIDIZE	[ ]	PERFORATE CASING	[ ]	SHOOTING OR ACIDIZING	[ ]	ALTERING CASING	[ ]
REPAIR WELL	[ ]	CHANGE PLANS	[ ]			ABANDONMENT	[ ]
(OTHER)			[ ]	(OTHER)			[ ]

(NOTE: Report results of multiple completion on Well Completion or Recompletion Report and Log form.)

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TITE HOLE - CONFIDENTIAL

Week of July 10 through July 16, 1982.

Drld to 7099'. Trip for washout 1' above pin 39th jt. Drld to7104'. Trip for washout 1' above pin 55th jt. Drld to 7238'. Trip for bit. Drld to 7350'. Trip for washout 1 jt above pin on 189th jt DP. Drld to 7474', 50 std trip to recover parted survey wireline. Drld to 7591'. Trip for washout 1' above pin in 119th jt DP. Drld to 7700'. Started testing BOP's. Surveys - 4-1/4 deg at 6993', 4 deg at 7115', 3-3/4 deg at 7236', 3-1/2 deg at 7367', 4-1/2 deg at 7457', 3-1/2 deg at 7489', 3-3/4 deg at 7584', 2-1/2 deg at 7700'. Mud 9.1, Vis 36, WL 13.6.

8. I hereby certify that the foregoing is true and correct.

Signed M. K. Smart for D. Fisher
D. J. Fisher

Title Area Manager Date 7/16/82

Permit No. 796.

STATE OF ARIZONA
OIL & GAS CONSERVATION COMMISSION
Sundry Notices and Reports On Wells
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JUL 15 1982
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SUNDRY NOTICES AND REPORTS ON WELLS

1. Name of Operator: Phillips Petroleum Company
2. OIL WELL [X] GAS WELL [ ] OTHER [ ] (Specify)
3. Well Name: Mountain View State "A" No. 1
   Location: 2630' FNL & 1860' FEL
   Sec. 10 Twp. 17S Rge. 15E County Pima, Arizona.
4. Federal, State or Indian Lease Number, or lessor's name if fee lease: State Lease #51389
5. Field or Pool Name: Wildcat
6. Check Appropriate Box to Indicate Nature of Notice, Report, or Other Data

NOTICE OF INTENTION TO:				SUBSEQUENT REPORT OF:			
TEST WATER SHUT-OFF	[ ]	PULL OR ALTER CASING	[ ]	WATER SHUT-OFF	[ ]	~~MONTHLY~~ Weekly PROGRESS	[XX]
FRACTURE TREAT	[ ]	DIRECTIONAL DRILL	[ ]	FRACTURE TREATMENT	[ ]	REPAIRING WELL	[ ]
SHOOT OR ACIDIZE	[ ]	PERFORATE CASING	[ ]	SHOOTING OR ACIDIZING	[ ]	ALTERING CASING	[ ]
REPAIR WELL	[ ]	CHANGE PLANS	[ ]			ABANDONMENT	[ ]
(OTHER)			[ ]	(OTHER)			[ ]

(NOTE: Report results of multiple completion on Well Completion or Recompletion Report and Log form.)

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TITE HOLE - CONFIDENTIAL

Week of July 3 through July 9, 1982 -

Drld to 6553'. Tstd BOP's to 2000 psi, OK, Hydril to 1500 psi, OK. Drld to 6676'. Wireline parted while running survey at 6676'. Made partial trip to rec Totco. Drld to 6800'. Trip for washout in 118th jt of DP. Drld to 6838'. Trip for washout in slip area of 25th jt of DP. Trip for bit. Inspected BHA. Drld to 6924'. Trip for washout in box of 11th DC. Surveys - 4 deg at 6460', 4-3/4 deg at 6708', 4-3/4 deg at 6835', 4-1/2 deg at 6904'. Mud 9.0, Vis 30, WL 12..

8. I hereby certify that the foregoing is true and correct.

Signed D J Fisher
D. J. Fisher
Title Area Manager Date 7/9/82

Permit No. 796

STATE OF ARIZONA
OIL & GAS CONSERVATION COMMISSION
Sundry Notices and Reports On Wells
File One Copy
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SUNDRY NOTICES AND REPORTS ON WELLS

1. Name of Operator Phillips Petroleum Company
2. OIL WELL [X] GAS WELL [ ] OTHER [ ] (Specify)
3. Well Name Mountain View State "A" No. 1
   Location 2630' FNL and 1860' FEL
   Sec. 10 Twp. 17S Rge. 15E County Pima, Arizona.
4. Federal, State or Indian Lease Number, or lessor's name if fee lease State Lease #51389
5. Field or Pool Name Wildcat
6. Check Appropriate Box to Indicate Nature of Notice, Report, or Other Data

NOTICE OF INTENTION TO:				SUBSEQUENT REPORT OF:			
TEST WATER SHUT-OFF	[ ]	PULL OR ALTER CASING	[ ]	WATER SHUT-OFF	[ ]	weekly ~~XXXXXXXX~~ PROGRESS	[XX]
FRACTURE TREAT	[ ]	DIRECTIONAL DRILL	[ ]	FRACTURE TREATMENT	[ ]	REPAIRING WELL	[ ]
SHOOT OR ACIDIZE	[ ]	PERFORATE CASING	[ ]	SHOOTING OR ACIDIZING	[ ]	ALTERING CASING	[ ]
REPAIR WELL	[ ]	CHANGE PLANS	[ ]			ABANDONMENT	[ ]
(OTHER)			[ ]	(OTHER)			[ ]

(NOTE: Report results of multiple completion on Well Completion or Recompletion Report and Log form.)

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TITE HOLE - CONFIDENTIAL

Week of June 26 thru July 2, 1982

Drld to 5456', trip for bit. Drld to 5503'. Tested BOP, manifold, Kelly and rams to 2000 psi, OK. Tested hydril to 1500 psi. Drld to 6194'. Trip for bit. Drld to 6361'. Trip for washout in slip area of 138th jt DP. Surveys - 3 deg at 5456', 2-3/4 deg at 5557', 3-1/4 deg at 5743', 4-1/3 deg at 5929', 4-1/2 deg at 6116', 4-3/4 deg at 6270' and 4-1/4 deg at 6333'. Mud 9.1, Vis 29, WL 12.8.

8. I hereby certify that the foregoing is true and correct.

Signed D. J. Fisher Title Area Manager Date 7/2/82

Permit No. 796

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OIL & GAS CONSERVATION COMMISSION
Sundry Notices and Reports On Wells
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SUNDRY NOTICES AND REPORTS ON WELLS

1. Name of Operator: Phillips Petroleum Company
2. OIL WELL [X] GAS WELL [ ] OTHER [ ] (Specify)
3. Well Name Mountain View State "A" No. 1
   Location 2630' FNL & 1860' FEL
   Sec 10 Twp. 17S Rge. 15E County Pima, Arizona.
4. Federal, State or Indian Lease Number, or lessor's name if fee lease State Lease #51389
5. Field or Pool Name
6. Check Appropriate Box to Indicate Nature of Notice, Report, or Other Data

NOTICE OF INTENTION TO:

TEST WATER SHUT-OFF	[ ]	PULL OR ALTER CASING	[ ]
FRACTURE TREAT	[ ]	DIRECTIONAL DRILL	[ ]
SHOOT OR ACIDIZE	[ ]	PERFORATE CASING	[ ]
REPAIR WELL	[ ]	CHANGE PLANS	[ ]
(OTHER)			[ ]

SUBSEQUENT REPORT OF:

WATER SHUT-OFF	[ ]	weekly ~~MONTHLY~~ PROGRESS	[XXX]
FRACTURE TREATMENT	[ ]	REPAIRING WELL	[ ]
SHOOTING OR ACIDIZING	[ ]	ALTERING CASING	[ ]
		ABANDONMENT	[ ]
(OTHER)			[ ]

(NOTE: Report results of multiple completion on Well Completion or Recompletion Report and Log form.)

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TITE HOLE - CONFIDENTIAL

Week of June 19 - June 25, 1982

Drld to 4132'. Trip for bit. Tested BOP's, OK. Drld to 4958'. Trip for bit. Drld to 5372'. Surveys - 3-3/4 deg at 4128', 4-1/2 deg at 4253', 3-1/4 deg at 4437', 2-3/4 deg at 4623', 2-3/4 deg at 4812', 3 deg at 4997', 2-1/2 deg at 5184', and 2-3/4 deg at 5372'. Mud 9.2, Vis 29, WL 12.

I hereby certify that the foregoing is true and correct.

D. J. Fisher

Title Area Manager Date 6/25/82

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OIL & GAS CONSERVATION COMMISSION
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JUN 23 1982
O & G CONS. COMM.

SUNDRY NOTICES AND REPORTS ON WELLS

1. Name of Operator Phillips Petroleum Company

2. OIL WELL [X] GAS WELL [ ] OTHER [ ] (Specify)

3. Well Name Mountain View State "A" No. 1

Location 2630' FNL & 1860' FEL

Sec. 10 Twp. 17S Rge. 15E County Pima, Arizona.

4. Federal, State or Indian Lease Number, or lessor's name if fee lease State Lease #51389

5. Field or Pool Name Wildcat

6. Check Appropriate Box to Indicate Nature of Notice, Report, or Other Data

NOTICE OF INTENTION TO:				SUBSEQUENT REPORT OF:			
TEST WATER SHUT-OFF	[ ]	PULL OR ALTER CASING	[ ]	WATER SHUT-OFF	[ ]	weekly ~~MONTHLY~~ PROGRESS	[XXX]
FRACTURE TREAT	[ ]	DIRECTIONAL DRILL	[ ]	FRACTURE TREATMENT	[ ]	REPAIRING WELL	[ ]
SHOOT OR ACIDIZE	[ ]	PERFORATE CASING	[ ]	SHOOTING OR ACIDIZING	[ ]	ALTERING CASING	[ ]
REPAIR WELL	[ ]	CHANGE PLANS	[ ]			ABANDONMENT	[ ]
(OTHER)			[ ]	(OTHER)			[ ]

(NOTE: Report results of multiple completion on Well Completion or Recompletion Report and Log form.)

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TITE HOLE - CONFIDENTIAL

~~Week of~~ June 12 through June 18

Drld to 2854'. Trip for bit. Drld to 3334'. Trip for bit. Drld to 3897'. Surveys - 1-1/2 deg at 1521', 1-1/4 deg at 1707', 3/4 deg at 2047', 1 deg at 2169', 1-1/4 deg at 2511', 1-1/2 deg at 2854', 2 deg at 3070', 3285', 3412', 3506', 2-1/2 deg at 3880'. Mud 9.0, Vis 36, WL 8.8..

8. I hereby certify that the foregoing is true and correct.

Signed M. K. Widsher for Fisher Title Area Manager Date 6/18/82
D. J. Fisher

Permit No. 796

STATE OF ARIZONA
OIL & GAS CONSERVATION COMMISSION
Sundry Notices and Reports On Wells
File One Copy
Form No. 25

June 10, 1982

Phillips Pet. Mtn View A1 State (796)

6-8-82 Departed Phx @ 2:30 p.m.
Arrived @ Tucson @ 5:20 pm + checked in at the Desert Inn Motel @ Congress + Freeway

Failing to contact Rig via telephone, I drove out to Rig at 8:00 pm, following instructions as per drilling program. Was unable to get to Rig this nite and later managed to get thru to the Rig — job would be ready @ 7:00 am ± — were still drlg @ 11:30 pm, final few feet (T.D. 1055')

6-9-82 Checked out of Motel + departed for Rig at 7:30 am + got there at 8:15 am — loggins compl'd @ 6:00 am + were conditioning hole. Ran 9 5/8", 40#, K-55 csg to 1071'. Halliburton conditioned hole + cemented, using ± 612 Sx of diacel mix, chased w/ 120 Sx of neat cement — got returns to the surface. Job finished ± 12:00 pm Left Rig @ 12:45 pm + stopped @ Bureau of Geo + Minerals tech. office (Geth.) + visited briefly w/ Claudia Stone + Jim Witcher. Picked up 2 copies of State Geothermal Resources map (fresh off the press) — called in office @ 2:45 pm + left for Phx @ 3:00 pm

Arrived @ 5:30 pm

(542 miles)

RECEIVED

JUN 14 1982

O & G CONS. COMM.

SUNDRY NOTICES AND REPORTS ON WELLS

1. Name of Operator Phillips Petroleum Company

2. OIL WELL [X] GAS WELL [ ] OTHER [ ] (Specify)

3. Well Name Mountain View State "A" No. 1

Location 2630' FNL & 1860' FEL

Sec 10 Twp. 17S Rge. 15E County Pima, Arizona.

4. Federal, State or Indian Lease Number, or lessor's name if fee lease State Lease #51389

5. Field or Pool Name Wildcat

6. Check Appropriate Box to Indicate Nature of Notice, Report, or Other Data

NOTICE OF INTENTION TO:				SUBSEQUENT REPORT OF:			
TEST WATER SHUT-OFF	[ ]	PULL OR ALTER CASING	[ ]	WATER SHUT-OFF	[ ]	weekly ~~WEEKLY~~ PROGRESS	[X]
FRACTURE TREAT	[ ]	DIRECTIONAL DRILL	[ ]	FRACTURE TREATMENT	[ ]	REPAIRING WELL	[ ]
SHOOT OR ACIDIZE	[ ]	PERFORATE CASING	[ ]	SHOOTING OR ACIDIZING	[ ]	ALTERING CASING	[ ]
REPAIR WELL	[ ]	CHANGE PLANS	[ ]			ABANDONMENT	[ ]
(OTHER)			[ ]	(OTHER)			[ ]

(NOTE: Report results of multiple completion on Well Completion or Recompletion Report and Log form.)

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TITE HOLE - CONFIDENTIAL

Week of June 6 thru June 11

INITIAL REPORT. 9,000' Paleozoic structural strat exploratory test well. MI and RURT 6/6/82. Spudded 12-1/4 inch surf hole at 6:00 P.M., 6/6/82. Drld to 581'. Trip for plugged jets. PU new bit. Drld to 620'. Work stuck pipe, came free. Drld to 966'. Trip for bit, Drld to 1080'. Circ and cond hole. COOH. RU Schl., ran DIL-SP-GR and BHC-SONIC-CAL from TD to surface. RD Schl. LD 8 inch DC. Start RU to run csg. Ran 25 jts 9-5/8 in 40 lb K-55 ST and C csg set at 1071'. Circ. Cmtd w/500 gal Flochek, followed w/478 sx class G w/10 percent diacel D and 2 percent gel at 12.8 PPG. Full returns. Circ 25 sx excess. Plug down at 10:45 A.M., 6/9/82. NU. Tested BOP's and manifold to 2000 psi, hydril to 1500 psi, OK. LDDP. PU DC. PU DP. Drld cmt plug. Press test csg 1000 psi, OK. Drld 7-7/8 inch hole to 1497'. Surveys - 3/4 deg at 296', 1/4 deg at 568', 0 deg at 754', 3/4 deg at 877', 1/2 deg at 1080', 1-1/4 deg at 1269', 1-1/4 deg at 1426'. Mud 8.8, Vis 31, WL 12.

8. I hereby certify that the foregoing is true and correct.

Signed D. J. Fisher Title Area Manager Date 6/11/82

Permit No 796

STATE OF ARIZONA
OIL & GAS CONSERVATION COMMISSION
Sundry Notices and Reports On Wells
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Form No. 25

PHILLIPS PETROLEUM COMPANY

P.O. Box 2920
Casper, WY 82602

RECEIVED
MAY 13 1982
O & G CONS. COMM.

May 10, 1982

To: A.K. Doss, AZ O & G.

Mr. A. L. Michaelis
Box 178
Evanston, Wyoming 82930

RE: Mountain View "A" No. 1

The following pertains to drilling the subject "Strat Test".

Status: Tight Hole
AFE: P-U714
API No. 02-019-20015
Location: 2630' FNL & 1860' FEL, Sec. 10-T17S-R15E,
Pima County, Arizona

Project T. D. - 9,000'

State Archaeological - cleared
State Agriculture & Horticulture - in progress

Well Site Directions: Well site is approximately 15 miles S.E. of Tucson. Drive SE of Tucson on I-10 about 10 miles to Houghton interchange, then 8 miles south through Coronas de Tucson, then one mile west on blacktop to rig sign and 1.5 miles north on newly constructed road along power line and then 0.3 miles west to location.

Surface: Edmond Layton, Rt. 7 Box 828, Tucson, Arizona 85706

Lease: Arizona State #51389

Drilling Contractor: Brinkerhoff-Signal No. 9 (Farmington, New Mexico (505) 327-5025).

Water: Purchase and haul.

Communications: Motorola Radio link from B'Ville Comm. Contact is Ed Gilliland (918) 661-9058. Back up is Don Ballew (918) 661-8199.
Local Service contact for installation and maintenance is Motorola Service Station, Tucson, Arizona, Art Lippolis, Mgr. (602) 624-4423.
Business Radio License KNBJ-928 covers. Rig Phone number (602)_____ -_____
Datotek scramblers will be provided.

RECEIVED
FEB 1 1982
O & G CONS. COMM.

APPLICATION FOR PERMIT TO DRILL OR RE-ENTER

APPLICATION TO DRILL ☒ STRAT TEST RE-ENTER OLD WELL ☐

PHILLIPS PETROLEUM COMPANY
NAME OF COMPANY OR OPERATOR

P.O. Box 2920 | Casper, | Wyoming 82602
Address | City | State

Loffland Brothers Company
Drilling Contractor

P.O. Box 3565, Grand Junction, Colorado 81501
Address

DESCRIPTION OF WELL AND LEASE

Federal, State or Indian Lease Number, or if fee lease, name of lessor: State Lease #51389 (Mtn View State)	Well number: A#1	Elevation (ground): 3086 (est)
Nearest distance from proposed location to property or lease line: 660 feet	Distance from proposed location to nearest drilling, completed or applied-for well on the same lease: None on this lease feet	
Number of acres in lease: 2080.08	Number of wells on lease, including this well, completed in or drilling to this reservoir: 1	
If lease, purchased with one or more wells drilled, from whom purchased: N/A	Name	Address
Well location (give footage from section lines): 2630 FNL & 1860 FEL sw ne	Section—township—range or block and survey: 10-T17S-R15E G&SRM	Dedication (Comply with Rule 105): 80 Acres
Field and reservoir (if wildcat, so state): Wildcat	County: PIMA	
Distance, in miles, and direction from nearest town or post office: 14 miles SE of Tucson, AZ.		
Proposed depth: 9000'	Rotary or cable tools: Rotary	Approx. date work will start: 5/15/82
Bond Status on file Amount $25,000	Organization Report On file X Or attached	Filing Fee of $25.00 Attached X

Remarks: Well information confidential

CERTIFICATE: I, the undersigned, under the penalty of perjury, state that I am the Area Manager of the Phillips Petroleum Company (company), and that I am authorized by said company to make this report; and that this report was prepared under my supervision and direction and that the facts stated therein are true, correct and complete to the best of my knowledge.

2- Arizona O&GC
1-Bartlesville Prod
1 - T. J. Jobin
1 - File

Signature D. J. Fisher
D. J. Fisher

Date January 27, 1982

Permit Number: 496
Approval Date: 2-1-82
Approved By: [illegible]

Notice: Before sending in this form be sure that you have given all information requested. Much unnecessary correspondence will thus be avoided.

STATE OF ARIZONA
OIL & GAS CONSERVATION COMMISSION
Application to Drill or Re-enter
File Two Copies

Form No. 3

(Complete Reverse Side)

1. Operator shall outline the dedicated acreage for both oil and gas wells on the plat.

2. A registered professional engineer or land surveyor registered in the State of Arizona or approved by the Commission shall show on the plat the location of the well and certify this information in the space provided.

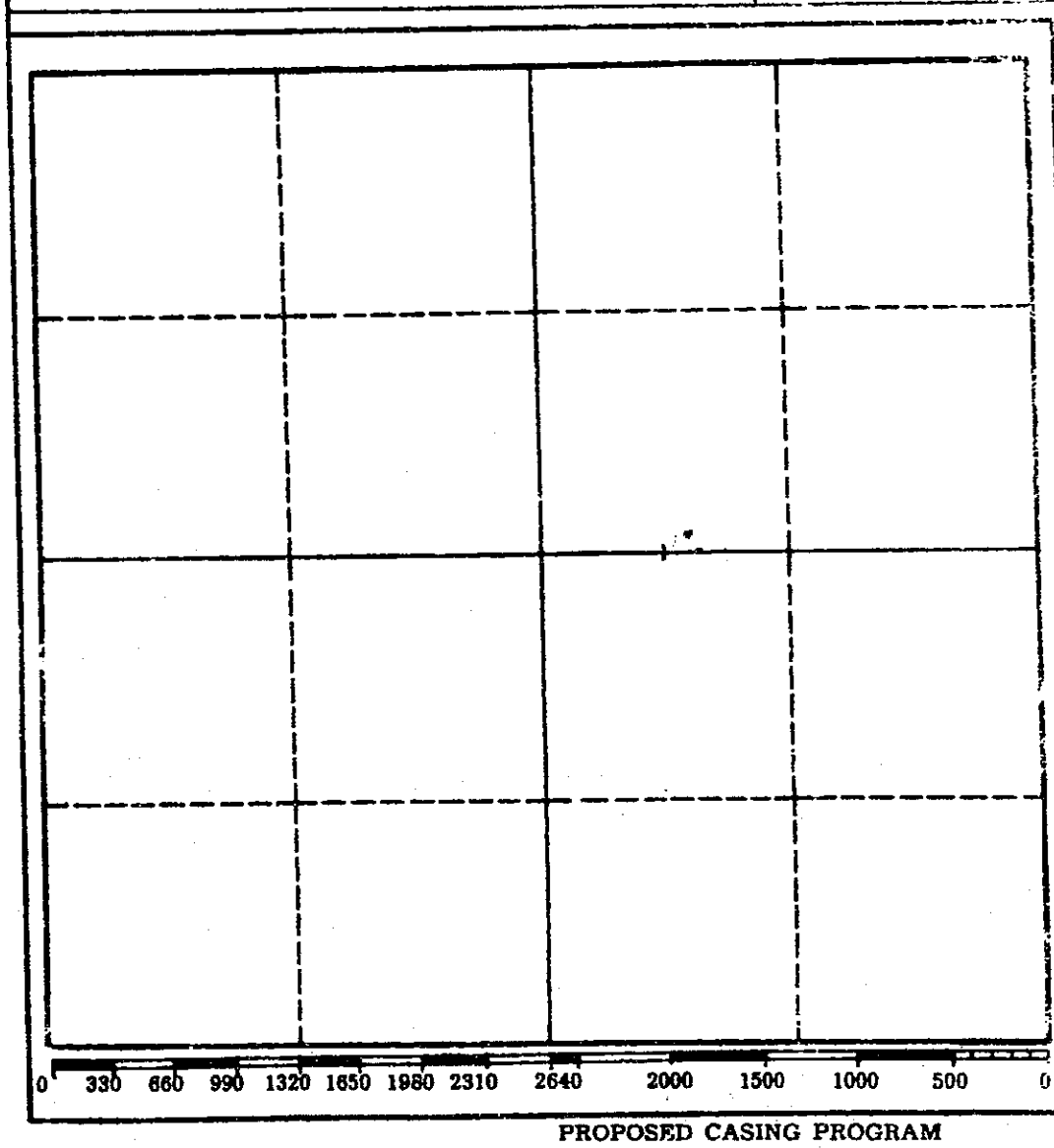
3. All distances shown on the plat must be from the outer boundaries of the Section.

4. Is the Operator the only owner in the dedicated acreage outlined on the plat below? YES____ NO X

5. If the answer to question four is "no," have the interests of all the owners been consolidated by communitization agreement or otherwise? YES. X NO____ If answer is "yes," Type of Consolidation Joint venture

6. If the answer to question four is "no," list all the owners and their respective interests below:

Owner	Land Description
Phillips, Et Al	Per lease #, reverse



CERTIFICATION

I hereby certify that the information above is true and complete to the best of my knowledge and belief.

Name: D. J. Fisher

Position: Area Manager

Company: Phillips Petroelum Co.

Date: January 27, 1982

I hereby certify that the well location shown on the plat was plotted from field notes of actual surveys made by me or under my supervision, and that the same is true and correct to the best of my knowledge and belief.

Date Surveyed: To be forwarded

Registered Professional Engineer and/or Land Surveyor

Certificate No.

PROPOSED CASING PROGRAM

Size of Casing	Weight	Grade & Type	Top	Bottom	Cementing Depths	Sacks Cement
9-5/8"	40#	K-55	Surf.	1000'±	0-1000'	As required

FORM F-106

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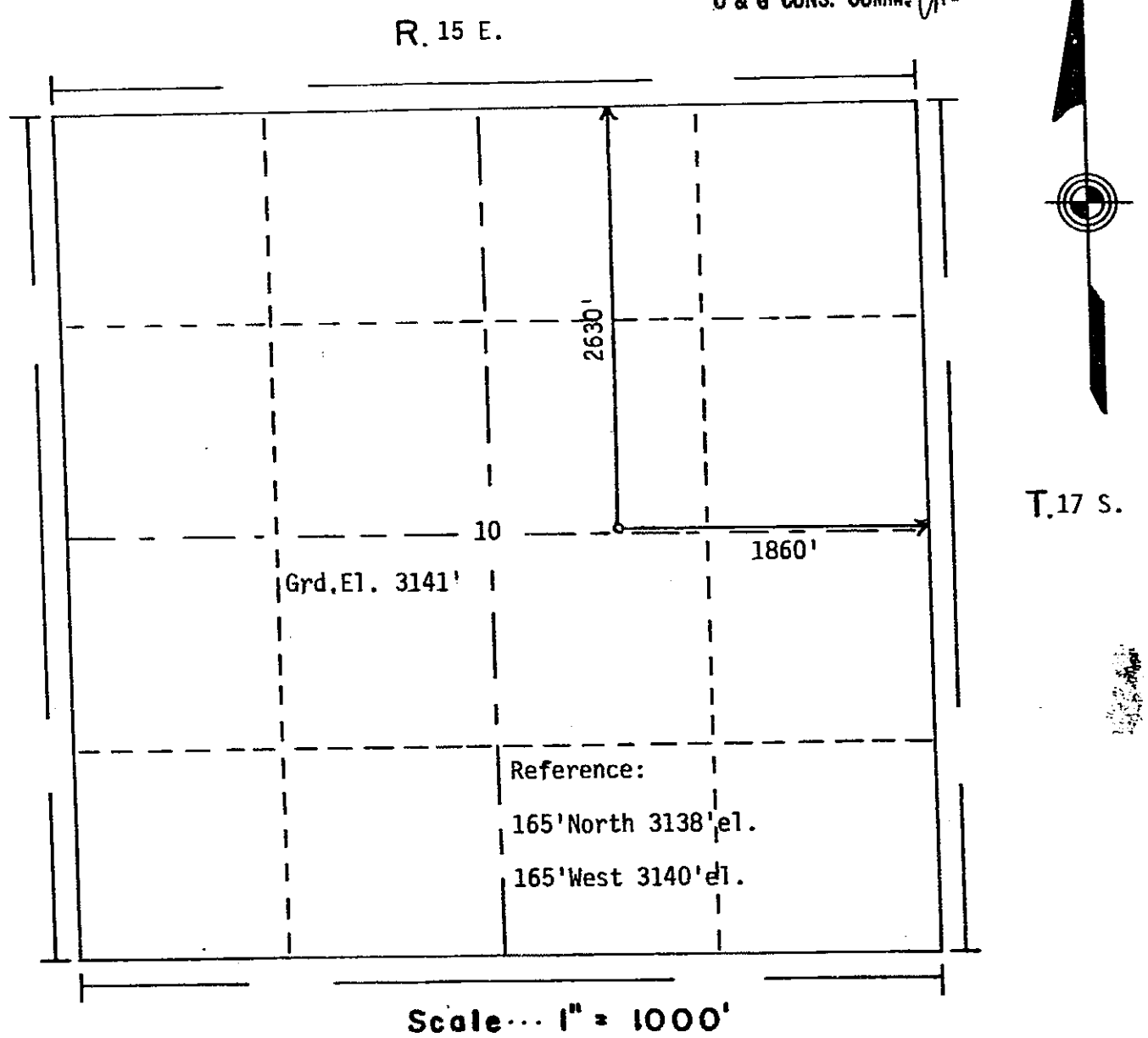
O & G CONS. COMM.



Scale··· 1" = 1000'

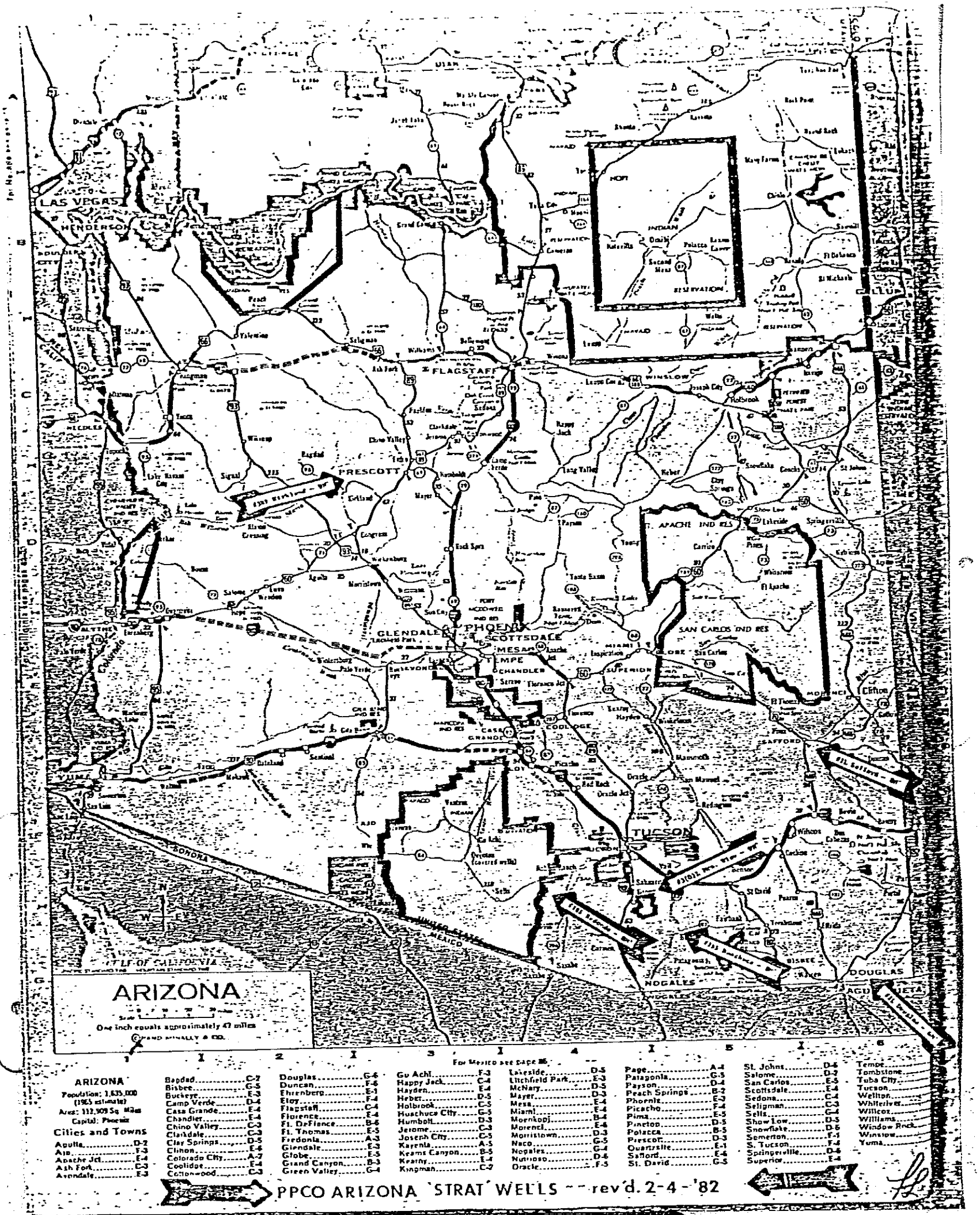
Powers Elevation of Denver, Colorado
has in accordance with a request from Frank Lyte
for Phillips Petroleum Company
determined the location of Mountain View
to be 2630' FNL & 1860' FEL Section 10 Township 17 South
Range 15 East Gila and Salt River Meridian
Pima County, Arizona

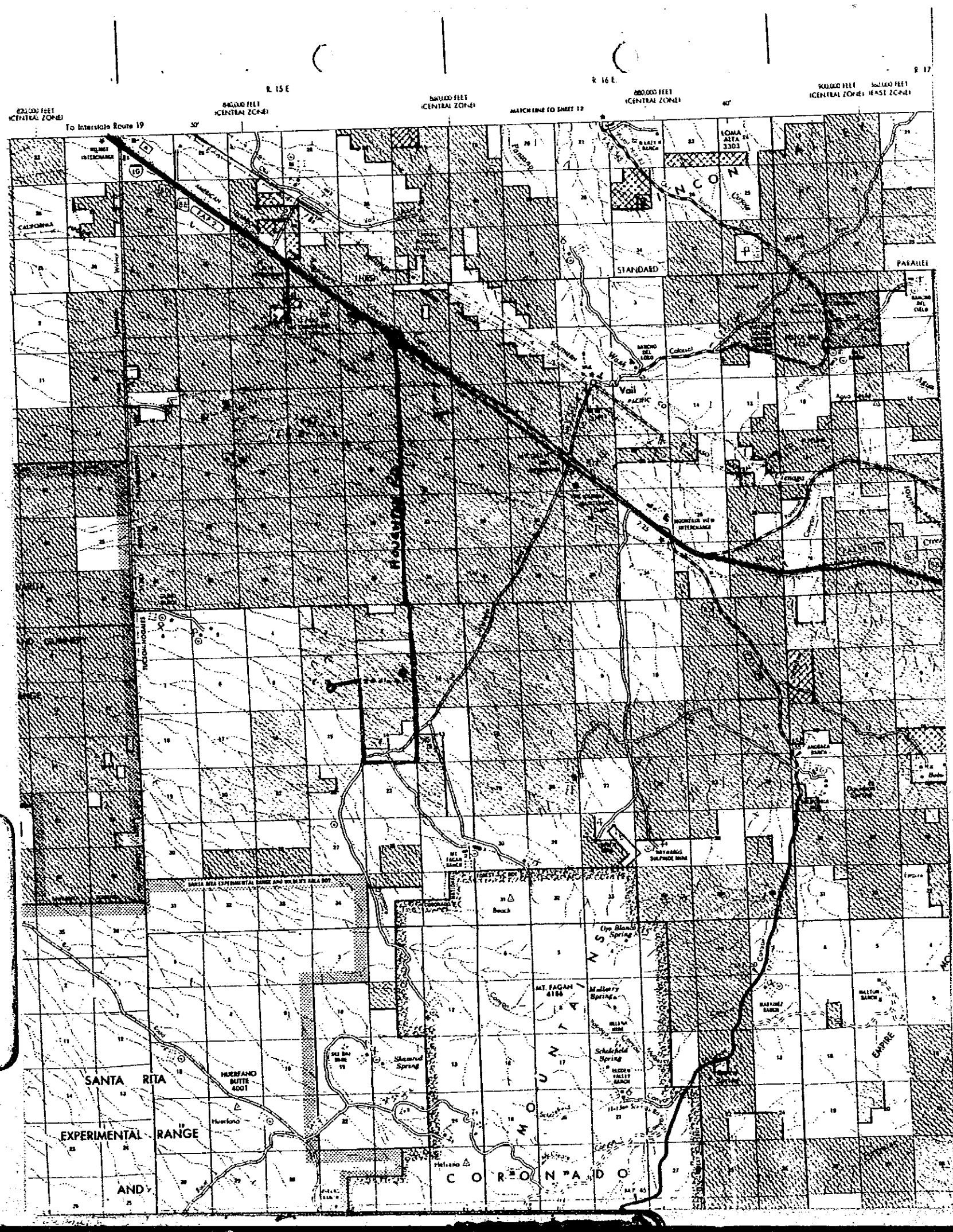
I hereby certify that this plat is an accurate representation of a correct survey showing the location of

Date: 18 May 1981

Licensed Land Surveyor No. 6844
State New Mexico

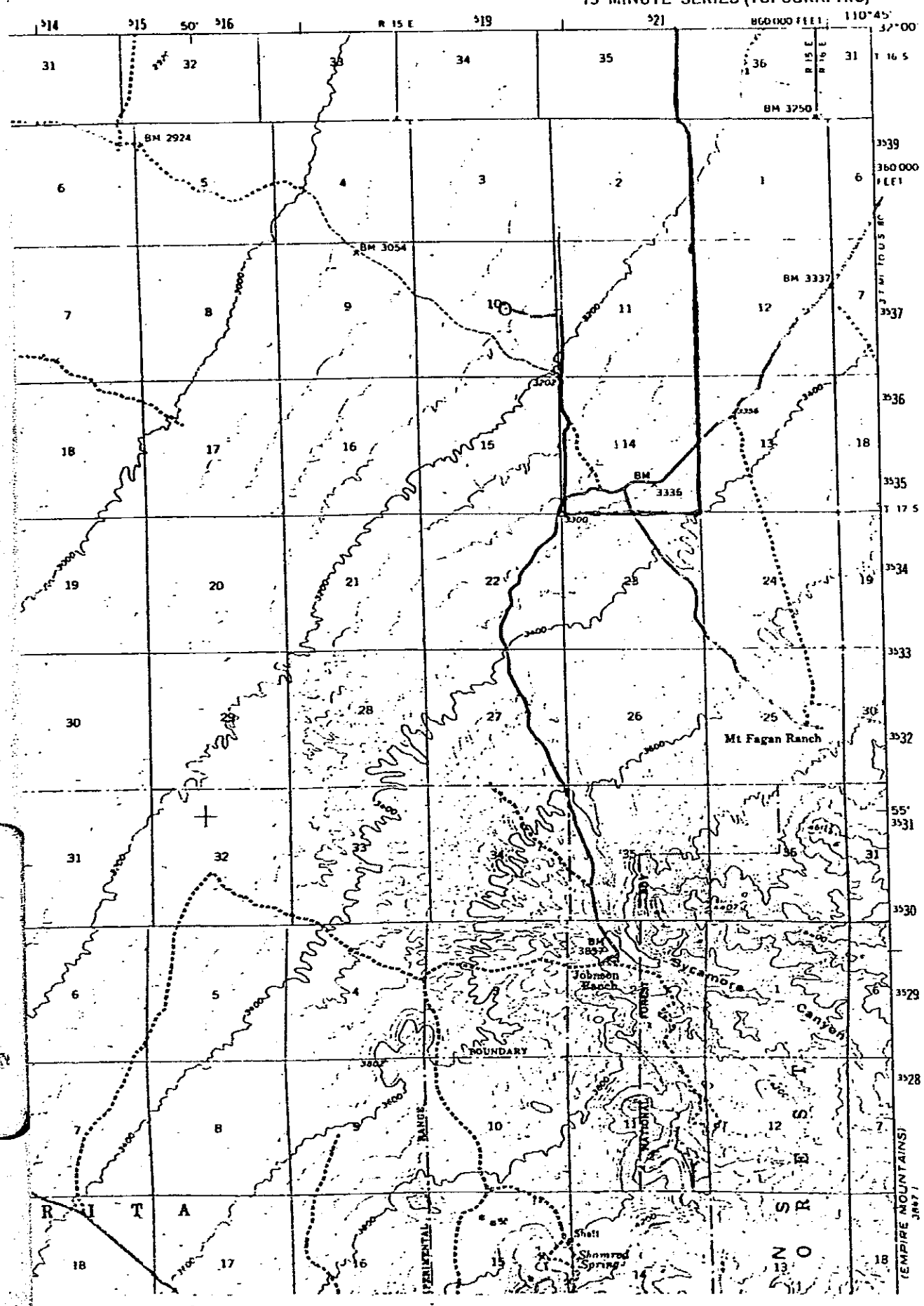
REGISTERED LAND SURVEYOR · NEW MEXICO · 6844

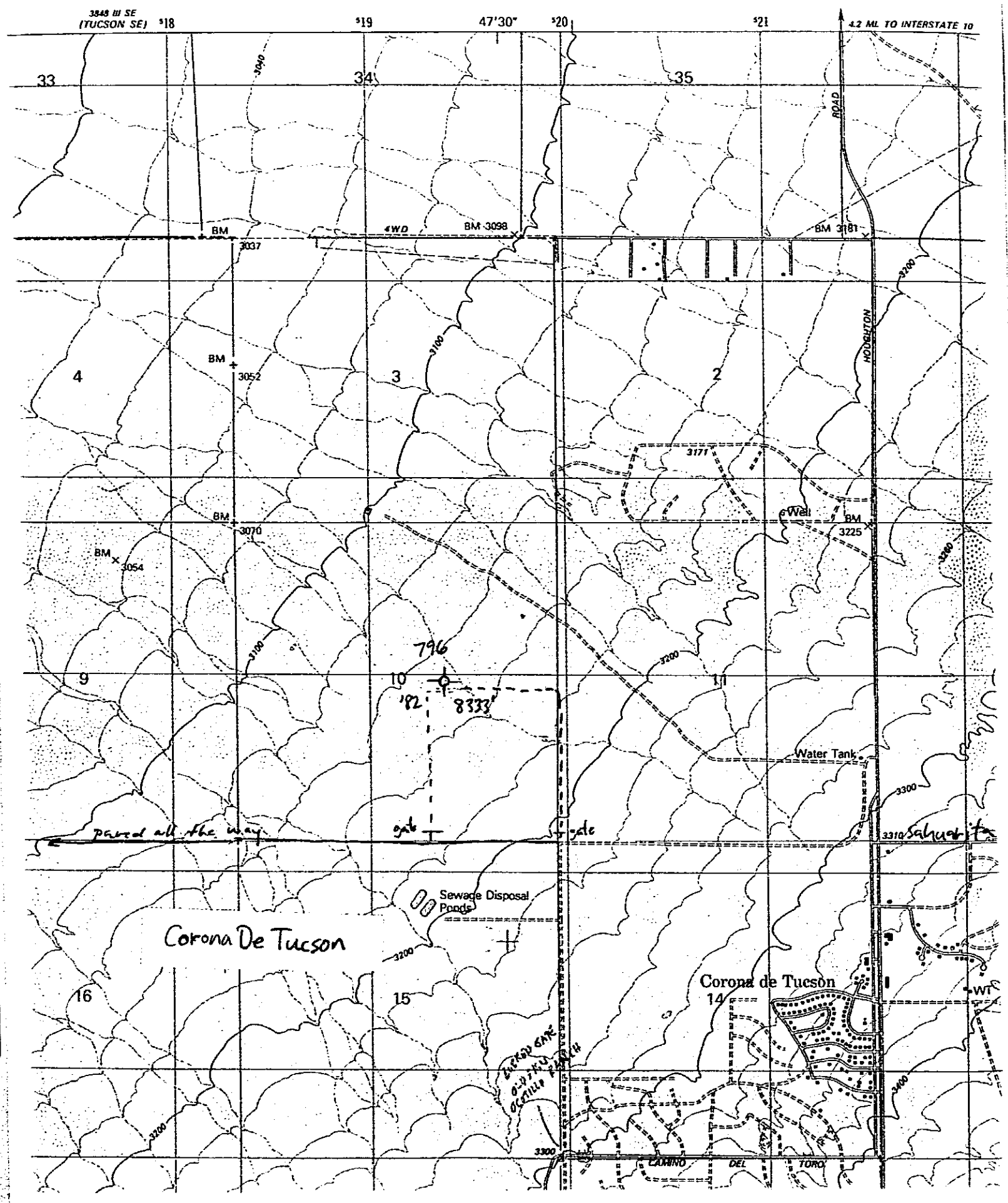

ARIZONA
One inch equals approximately 47 miles
LAS VEGAS
HENDERSON
FLAGSTAFF
PRESCOTT
PHOENIX
GLENDALE
SCOTTSDALE
MESA
TEMPE
CHANDLER
TUCSON
NOGALES
DOUGLAS
WINSLOW
HOPI INDIAN RESERVATION
APACHE IND RES
SAN CARLOS IND RES
COOLIDGE
SAFFORD
SUPERIOR
GLOBE
MIAMI
YUMA
SONORA
MEXICO
For Mexico see page 86
ARIZONA
Population: 1,635,000 (1965 estimate)
Area: 113,909 Sq. Miles
Capital: Phoenix
Cities and Towns
Apache Jct. E-4
Ash Fork C-3
Avondale E-3
Bagdad C-2
Bisbee G-5
Buckeye E-3
Camp Verde D-4
Casa Grande E-4
Chandler E-4
Chino Valley C-3
Clarkdale C-3
Clay Springs D-5
Clifton E-6
Colorado City A-2
Coolidge E-4
Cottonwood C-3
Douglas G-6
Duncan F-6
Ehrenberg E-1
Eloy E-4
Flagstaff C-4
Florence E-4
Ft. DeFiance B-6
Ft. Thomas E-5
Fredonia A-3
Glendale E-3
Globe E-5
Grand Canyon B-3
Green Valley G-4
Gu Achi F-3
Happy Jack C-4
Hayden E-4
Heber D-5
Holbrook C-5
Huachuca City G-5
Humboldt D-3
Jerome C-3
Joseph City C-5
Kayenta A-5
Kearns Canyon B-5
Kearny E-4
Kingman C-2
Lakeside D-5
Litchfield Park E-3
McNary D-5
Mayer D-3
Mesa E-4
Miami E-4
Moenkopi B-4
Morenci E-6
Morristown D-3
Naco G-5
Nogales G-4
Nutrioso D-6
Oracle F-5
Page A-4
Patagonia G-5
Payson D-4
Peach Springs B-2
Phoenix E-3
Picacho F-4
Pima E-5
Pinetop D-5
Polacca B-5
Prescott D-3
Quartzsite E-1
Safford E-6
St. David G-5
St. Johns D-6
Salome D-2
San Carlos E-5
Scottsdale E-4
Sedona C-4
Seligman C-3
Sells G-4
Show Low D-5
Snowflake D-6
Somerton F-1
S. Tucson F-4
Springerville D-6
Superior E-4
Tempe
Tombstone
Tuba City
Tucson
Wellton
Whiteriver
Willcox
Williams
Window Rock
Winslow
Yuma
PPCO ARIZONA 'STRAT' WELLS -- rev'd. 2-4-'82


R. 15 E.
R. 16 E.
R. 17
To Interstate Route 19
MATCH LINE TO SHEET 12
STANDARD
PARALLEL
Vail
SANTA RITA
EXPERIMENTAL RANGE
AND
CORONADO
EMPIRE

Houghton I Mt. View

SAHUARITA QUADRANGLE
ARIZONA–PIMA CO.
15 MINUTE SERIES (TOPOGRAPHIC)




7.5 MII
3848 III SE
(TUCSON SE)
47'30"
4.2 MI. TO INTERSTATE 10
ROAD
HOUGHTON
4WD
BM 3098
BM 3181
BM 3037
BM 3052
BM 3070
BM 3054
BM 3225
3171
Well
3200
3100
3040
3260
796
182
8333
Water Tank
3300
3310
Saharita
paved all the way
gate
Sewage Disposal Ponds
Corona De Tucson
Corona de Tucson
WT
3400
CAMINO DEL TORO
33
34
35
4
3
2
9
10
11
16
15
14

PERMIT TO DRILL

This constitutes the permission and authority from the

OIL AND GAS CONSERVATION COMMISSION,
STATE OF ARIZONA,

To: PHILLIPS PETROLEUM COMPANY
(OPERATOR)

to drill a well to be known as

MTN VIEW A1 STATE
(WELL NAME)

located 2630' FROM NORTH LINE & 1860' FROM EAST LINE (SW NE)

Section 10 Township 17 SOUTH Range 15 EAST, PIMA County, Arizona.

The N/A of said Section, Township and Range is dedicated to this well.

Said well is to be drilled substantially as outlined in the attached Application and must be drilled in full compliance with all applicable laws, statutes, rules and regulations of the State of Arizona.

Issued this 1st day of February, 19 82.

OIL AND GAS CONSERVATION COMMISSION

By [signature]
EXECUTIVE SECRETARY

PERMIT Nº 796

RECEIPT NO. 2217

API NO. 02-019-20015

State of Arizona
Oil & Gas Conservation Commission
Permit to Drill

FORM NO. 27

TEN FOOT SAMPLES ARE REQUIRED FROM SURFACE

796 #4206 -Bartlesville File Copy- 3/83

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JUL 27 1983
O & G CONS. COMM.

PHILLIPS PETROLEUM

VELOCITY SURVEY

with

CALCULATION OF SYNTHETIC SEISMOGRAM

Mountain View State #A-1
Pima County, Arizona

Permit # 796

CGG
Department of Development Geophysics
1475 Lawrence Street
Denver, Colorado 80202

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* * * *

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APPENDIX 2: Computer Listings of Results

FOREWORD

This report is organized in three parts. The first part concerns the Velocity Survey, including a field operation report and a description of the seismic data, processing sequence and results.

The second part concerns the Synthetic Seismogram with an overview of the processing sequence and a presentation of the results.

The third part includes comments, conclusions, and recommendations for future surveys. Seismic traces were processed by Steve Wong, and the Synthetic Seismogram was produced by Dave Horowitz. The report was prepared under the supervision of Gildas Omnes, Pat Hooyman, and Charlie Wu.

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PART ONE: THE VELOCITY SURVEY

A. Field Operation Report

1. General Information

a. Well Information

Name of the Well:	Mountain View State #A-1
Area:	Pima County, Arizona
Coordinates:	SEC 10, T17S, R15E
Ground Elevation:	3141 feet
Kelly Bushing Elevation:	3156 feet
DP Elevation:	3000 feet
Correction Velocity:	6714 ft/sec (measured at the well)
Depth of Casing:	1068 feet
Depth of Mud:	Not available

b. Survey Information

Date	07/19/81
Type of Survey:	Checkshot
Station Interval:	Variable
Survey Range:	50 to 8300 feet
Number of Stations:	38
Maximum Depth Under KB:	8300 feet
Distance Source-Wellhead	42 feet

2. Personnel

Party Chief/Senior Observer	Jean Yves Gaborit
Junior Observer:	David Karpinia
Logging Crew:	SCHLUMBERGER

3. Equipment

Source:	Land Air Gun (LST 1, 2-8 pops) & Dynamite (5 lbs)
Downhole Tool:	SIE 3D
Signature Probe:	14 Hz Geophone
Recording System:	SN 338B; Addit II

4. Recording Parameters

Sampling Rate:	2 milliseconds
Recording Length:	6 seconds
HC Filter:	125 Hz
LC Filter:	OUT
60 Hz. Notch:	IN

B. Results

1. Checkshots

a. Procedure

The downhole tool was lowered to the bottom of the well (8300 feet), and the Air Gun was positioned 42 feet away from the wellhead. As the tool was pulled up the well, we recorded the seismic trace at each of the 38 levels.

b. Time Picking

First, we demultiplexed the traces and produced a normalized raw section (see Figure 1). This normalized section shows a good signal-to-noise ratio, and there is no ambiguity in determining the first breaks.

The raw times were picked directly from the raw data after cross-correlation with a wavelet chosen from one of the first breaks (see Figure 2). The S/N is excellent.

The deeper times, (below 500 feet), were linearly corrected to vertical and used to calibrate the Sonic log for the Synthetic Seismogram (see Appendix 2).

The times from 50 feet to 500 feet were used to determine the weathering velocity.

c. Velocity Calculation

The average time of traces with the same depth (due to several pops at the same depth) was calculated and listed below in the column labeled "TIME".

DEPTH (ft) (below KB)	DEPTH (ft) (below GL)	DISTANCE (ft)	TIME (ms)	AVERAGE VELOCITY (ft/sec)
50	35	54.67	6.6	8283
100	85	94.81	11.9	7966
200	185	188.7	38.3	4953
300	285	288.1	63.0	4573
400	385	387.3	85.0	4556
500	485	486.8	103.25	4715

N.B. : Offset of Land Air Gun: 42 feet

The weathering velocity from surface to datum plane was determined by interpolating the above velocities, and was found to be 6714 ft/sec. (DP is at 156 feet below KB or 141 feet below GL).

2. Uphole (Dynamite) Survey

a. Procedure

This survey was performed 532 feet away from the well. Dynamite was exploded at various depths from 19 feet to 294 feet below ground level (GL) and a surface geophone 6 feet away from the shot hole recorded the seismic signal.

b. Time Picking

The raw times were picked directly from the raw data after cross-correlation with a wavelet chosen from one of the first breaks (see Figure 3 and 4). The times obtained from different geophones show slight variations (less than .5 ms). Two groups of nine 40 Hz geophones (channels 24 and 26) have almost identical first break times at all shot depths. Another group consists of nine 14 Hz geophones

(channel 25) showed arrival times .2 ms to .5 ms earlier than that of channel 24 and 26. The average time of these three channels was used in determining velocities.

c. Velocity Calculation

The table below gives the results of this survey:

DEPTH (ft) (below GL)	DISTANCE TRAVELED (ft)	TIME (ms)	AVERAGE VELOCITY (ft/sec)
19	19.9	14.2	1401
44	44.4	27.4	1620
69	69.3	32.8	2113
94	94.2	40.3	2337
119	119.2	47.0	2535
144	144	83.4	2697
169	169	61.0	2770
194	194	66.2	2931
219	219	72.7	3012
244	244	77.7	3140
269	269	83.4	3225
294	294	86.3	3406

The velocities obtained from this survey are much lower than the velocities measured in the well, and they were not used in determining the weathering velocity at the well. They should nevertheless be considered as accurate, the S/N is excellent and the TB system was checked before and after the survey.

3. Lateral Stepout Survey

a. Procedure

This survey entailed sending the borehole sonde to a depth of 500 feet. Maintaining a depth of 500 feet, the air gun took a series of pops at horizontal distances from the borehole of 100, 200, 300, 400 and 500 feet (see sketch in Oberserver's report). The sonde was then positioned at a level of 400 feet below KB, and the above procedure repeated. Also, the following levels: 300, 200 and 100 feet were performed with the same procedure.

b. Time Picking

The times for this survey were picked directly from the normalized raw data section (see Figure 5). Some of the traces were dead or very noisy and they were not used. The S/N is good on all others.

c. Velocity Calculation

The system and instrument delay was determined to be 30 ms. The time used for velocity calculation for each station was obtained by subtracting 30 ms from the time pick. The results are listed below.

For an OFFSET of 100 feet:

DEPTH (ft) (below KB)	DEPTH (ft) (below GL)	DISTANCE (ft)	TIME (ms)	AVERAGE VELOCITY (ft/sec)
400	385	397.8	137.6	2890.8
300	285	302.0	124.1	2433.8
200	185	210.3	103.1	2039.7
100	85	131.2	83.1	1578.8

For an OFFSET of 200 feet:

DEPTH (ft) (below KB)	DEPTH (ft) (below GL)	DISTANCE (ft)	TRANSIT TIME (ms)	AVERAGE VELOCITY (ft/sec)
300	285	348.2	135.0	2579.3
200	185	272.4	119.0	2289.1
100	85	217.3	100.9	2153.6

For an OFFSET of 300 feet:

DEPTH (ft) (below KB)	DEPTH (ft) (below GL)	DISTANCE (ft)	TRANSIT TIME (ms)	AVERAGE VELOCITY (ft/sec)
400	385	488.1	152.3	3204.9
300	285	413.8	137.0	3020.4
200	185	352.5	127.3	2768.7
100	85	311.8	123.2	2530.9

For offsets of 400 and 500 feet, the traces could not be used. These velocities are compatible with those determined by the uphole survey; values are about the same and in both cases they increase regularly with depth, whereas in the case of the well, velocity reaches a minimum at 400 feet. Compared to velocities between the well and the location of the uphole survey (532 feet from the well), near surface average velocities at the well are abnormally high and show a minimum at 400 feet versus a progressive increase with depth.

In agreement with Mark Frishman from PHILLIPS, it was decided to use the velocity measured at the well (6714 ft/sec) as the correc-

tion to DP velocity. Considering that the travel times measured in the well with the Land air gun at 42 feet from the wellhead are reliable, the decision was logical. A possibility remains that the anomalous near surface velocities observed at the well are due to temporary conditions, the invasion of near surface formations by fluids used during drilling could have increased the velocities. If such was the case, the average velocity to surface used for the calculation of the synthetic with multiples could be too high.

Plots X^2 and T^2 show that down to 300 feet the subsurface cannot be considered as made of horizontal layers characterized by constant velocities. There is obviously a high velocity zone affecting the ray paths linking the 200 and 300 foot depth and the surface station at 300 feet from the well.

Step Out Survey

Average Velocities

	X ft	T sec	X^2	T^2	V
Depth 100 ft	100	83.1×10^{-3}	10^4	6905×10^{-6}	3026 ft/sec
	200	100.9×10^{-3}	4×10^4	10180×10^{-6}	3180 ft/sec
	300	123.2×10^{-3}	9×10^4	15123×10^{-6}	
Depth 200 ft	100	103.1×10^{-3}	10^4	10629×10^{-6}	2914 ft/sec
	200	119.0×10^{-3}	4×10^4	14161×10^{-6}	4945 ft/sec
	300	127.3×10^{-3}	9×10^4	16205×10^{-6}	
Depth 300 ft	100	124.1×10^{-3}	10^4	15400×10^{-6}	3258 ft/sec
	200	135.0×10^{-3}	4×10^4	18225×10^{-6}	9587 ft/sec
	300	137.0×10^{-3}	9×10^4	18769×10^{-6}	

In such conditions absolute ties between the CDP section and the Synthetic Seismogram cannot be determined on the basis of a checkshot.

C. Additional Processing

In order to verify whether the results of the checkshot survey can be used to correlate with the seismic section and Synthetic Seismogram, the following steps were taken:

1. Shaping Deconvolution

An operator 225 ms in length was used for shaping deconvolution. After this step, the data quality was much better than the equalized raw data section.

2. Time Variant Filter and F-K Filter (Figure 8)

A time variant filter of (10,80) Hz at the beginning and (8,60) Hz at time 2000 ms was applied to the data after shaping deconvolution. After the first breaks are flattened, an F-K reject filter (-50,000 ft/sec, 50,000 ft/sec) was used to filter out the downgoing events, then a static correction was applied to put the upgoing events in their proper positions. The same F-K reject filter was used to filter out the upgoing events at the upgoing events' lined up position. Then static correction was applied to put the downgoing events in their proper positions.

3. Upgoing Events Stacked (see Plate SECTION-1)

After flattening, shaping deconvolution, time variant filter and F-K filtering, the upgoing events are stacked. These may be correlated with the seismic section and Synthetic Seismogram.

4. Downgoing Events Stacked (see Plate SECTION-2)

After flattening, shaping deconvolution, time variant filter and F-K filtering, the downgoing events are stacked. These can be used to correlate with the seismic section and Synthetic Seismogram provided the S/N is sufficient.

PART TWO: THE SYNTHETIC SEISMOGRAM

A. Wireline Log Preparation

The Sonic log was recorded by SCHLUMBERGER and digitized from a paper plot (scale 1/200th) from 1070 to 8300 feet below Kelly Bushing (KB). The SCHLUMBERGER Density log was also digitized from a 1/200th scale paper plot from 1100 to 8300 feet and sampled every foot. The Sonic was extended to ground level (GL) with a constant velocity of 6900 ft/sec to enable calculation of multiples. Transit times of the Sonic log were integrated in order to obtain the depth at every 1 ms, and the Sonic times were compared to the seismic checkshot times.

B. Drift Corrections (see Plate SYN-1)

The difference between seismic times (seismic time minus sonic time) and integrated Sonic times (drift), was calculated for each checkshot station. These drift values were plotted versus depth, and the corrections applied were determined by using the optimum broken line plotted through the drift points.

At each slope change, depths (below KB) and drift values were picked. In order to adjust the Sonic times to match the seismic times, the following corrections were used:

DEPTH(ft) below KB	DRIFT CORRECTION(msec) added to Sonic time
1070	0
2020	-36.5
2490	-71
3130	-105
5665	-203
6135	-211
8300	-216.3
8311.73	-216.3

C. Results

The resulting Drift Plot and continuous velocity log (CVL) are presented on Plate SYN-1. The plot labeled "CHECKSHOTS" presents the Sonic log as a velocity log, scaled from 5000 to 20,000 ft/sec on a logarithmic grid. The plot has a linear time scale (two-way time), and the corresponding depth scale is presented on the far left. In addition, the checkshots are located on the plot according to: vertical depth below KB, vertical seismic time below datum plane (DP), and adjusted Sonic time below DP. Here only six of the 38 checkshots are presented, at the six points of drift correction.

The other half of Plate SYN-1 is the final Drift Plot, with the drift value at each checkshot indicated by a small "+". The broken line shows the actual value of drift added to the Sonic time at each depth.

Plate SYN-2 serves to compile all the various velocity functions, plotted with a linear depth scale. At the far left of Plate SYN-2 the checkshot stations and three formation tops are located by depth. Then we have five curves describing various parameters. Starting from the left side, the first curve is a plot of the integrated, adjusted CVL with a linear velocity scale from 2000 to

30,000 ft/sec. Next is a plot of the Sonic log integration, or the time traveled at every depth. The last three curves show the average velocity, the RMS velocity, and the interval velocity between stations.

Plate SYN-3 is a compilation of the wireline logs used plus the adjusted CVL, acoustic impedance, and reflection coefficients, all plotted with a linear depth scale.

To complement this is Plate SYN-4, which shows the wireline logs plus the velocity and acoustic impedance curves plotted with a linear time scale.

D. The Synthetic

The computation of a Synthetic Seismogram assumes that:

- the source and receiver are situated at the same point on the surface,
- the layers are horizontal,
- the waves are plane and horizontal at the point where they reach the surface.

The Synthetic Seismogram represents the sequence of reflection coefficients "K" computed with the following formula:

$$K = \frac{\rho_1 v_1 - \rho_2 v_2}{\rho_1 v_1 + \rho_2 v_2}$$

where ρ = density and v = velocity of layers 1 and 2. If the density is not available, d is taken as a constant.

With this formula an increase in acoustic impedance from layer 1 to layer 2 corresponds to a negative K, so in order to agree with S.E.G. polarity standards, the traces are reversed. Therefore, on Plates SYN-5 the "direct polarity" traces show an increase in acoustic impedance as a positive peak, agreeing with the S.E.G. polarity conventions.

The Synthetic Seismogram with multiples is computed with the surface as the origin of all times. Then the necessary correction is applied so that Plates SYN-5 show zero time at the datum plane of 3000 feet, to correlate with the seismic section and velocity survey.

On Plates SYN-5, the traces with direct polarity are presented on the left and those with reverse polarity are on the right. SSK refers to the Synthetic traces without multiples, and the traces labeled SSM have multiples included. Different values of surface reflection coefficients are used for computation of the Synthetic Seismogram with multiples. Here we used K = 0.0 and K = -.3, the first giving no surface multiples, and the second giving fairly strong surface multiples. Internal multiples (pegleg and interbed) are the same on all SSM plots.

Finally, the SSK and SSM traces are convolved with four different operators: "i" refers to the impulsional (or unfiltered)

trace, S1 used a (8,12,30,40) Hz, S2 used a (8,12,45,55) Hz, and S3 used a (8,12,60,80) Hz zero-phase bandpass filter. Eight traces of each convolution are presented as "wiggle" traces with shading on the peaks. For this survey, Plate SYN-5a is a full-scale plot with a 5 in/sec time scale, and SYN-5b is plotted at half-scale, or 2.5 in/sec.

Plate SYN-6 presents the Sonic and Density logs, one trace of each convolution, and eight "wiggle" traces of the convolutions. Again, the datum plane at 3000 feet occurs at zero time. On the left of SYN-6 are the wavelets and amplitude spectra of the filters used. In addition, three formation tops are labeled at their proper depths.

Plate SYN-7 is simply a comparison of one trace of each convolution with and without automatic volume control (AVC). This AVC is a gain applied to bring up the amplitude of the multiples. Below each set of traces is a plot of the gain in dB applied to the multiples. For this Synthetic, a large gain was applied, because the multiple reflections were very weak to begin with.

E. Computer Listings of Results

Appendix 2 consists of two computer printouts. The first, titled "Velocity Survey Computation Forms", is the result of the vertical time computation. The column labeled "DGR" is the depth below KB of each checkshot. Column "T" shows the time picked for the first break. This is multiplied by the "COS" of the angle between vertical and the actual source location to give "T2". Finally we add "TI" to adjust the seismic times back to the datum plane, taking into account the instrument delay and signature probe delays. This resultant vertical time is listed in column "T3", and the average seismic time (when more than one measurement was made on a level) is listed in column "T3M". "T3M" values are the vertical seismic times to which the Sonic times were corrected.

The second computer printout, titled "Listings of Results", comes from the final Synthetic computation. After the "List of Symbols," we have the formulae for drift corrections as well as the drift values used and the resulting corrected Sonic times. The rest of the printout shows the depth, velocity, and "K" (reflection coefficient) values for every millisecond, one-way time. Finally, the two tables at the very end give the depths, times and velocities at the checkshot stations. The value of "E" is the remaining difference between seismic and Sonic times after all the corrections have been applied. This number is our last quality check on our corrections, and we see that "E" is very close to zero, within one millisecond.

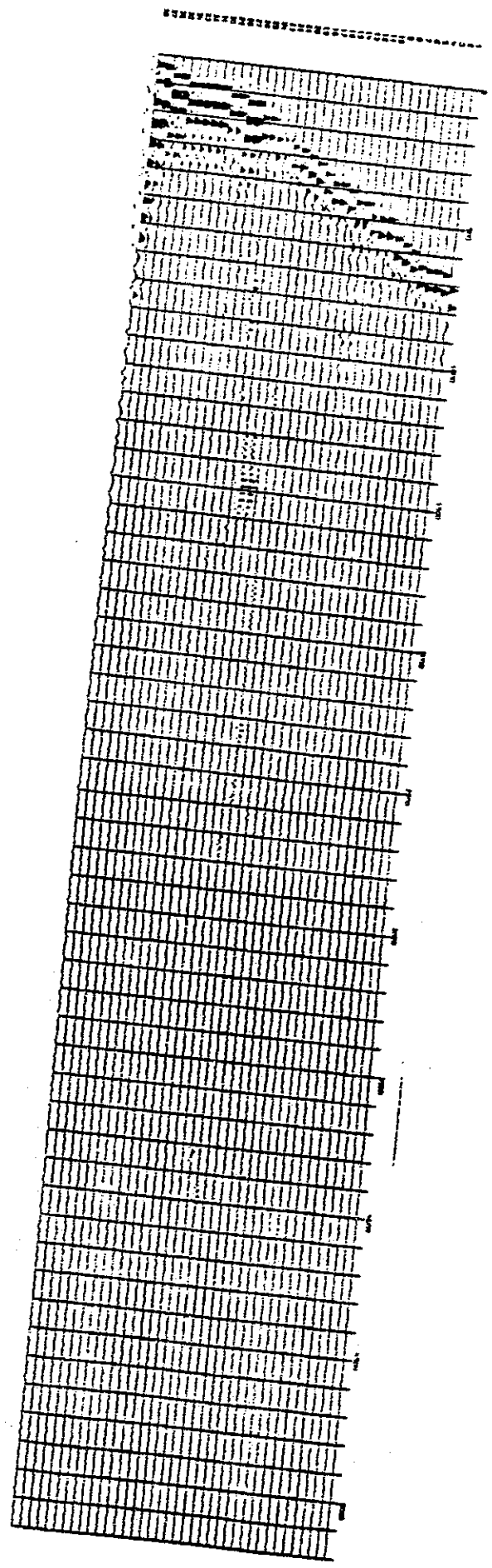
PART THREE: COMMMENTS, CONCLUSIONS AND RECOMMENDATIONS

The Mountain View State #A-1 velocity survey gave reliable results and the S/N for all first arrivals is good. A study of near surface velocities was carried out and it showed that strong lateral changes of velocities are present. The question was raised whether the anomalous velocities observed at the well when the source is off-set by 42 feet are due to the invasion of near surface formations by fluids spilled during drilling.

In any case, the step out velocity study showed that lateral velocity changes make absolute ties of a CDP section and a Synthetic Seismogram inaccurate.

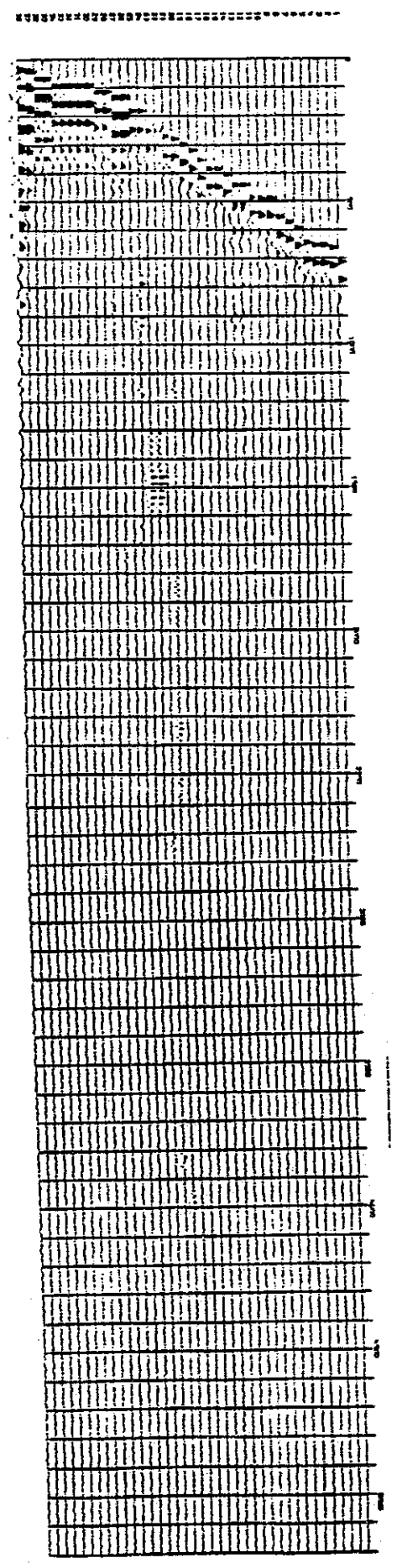
The processing and display of seismic traces VSP fashion show few obvious line-ups on the displays of flattened upgoing reflections, although a line-up over 4 traces at 680 ms coincides with a strong reflection coefficient on the calculated impedance log. Another coincidence occurs at 810 ms and the top of the granite at 1210 ms may be visible on the display. As a matter of fact, the correlation between the stack trace and the Synthetic Seismogram without multiples is rather good between 400 and 1250 ms.

FIGURE 1



NORMALIZED RAW DATA
OF CHECKSHOT

FIGURE 1



NORMALIZED RAW DATA
OF CHECKSHOT

FIGURE 2a

CROSS-CORRELATION OF CHECKSHOT
(PT1 - PT25), NORMALIZED

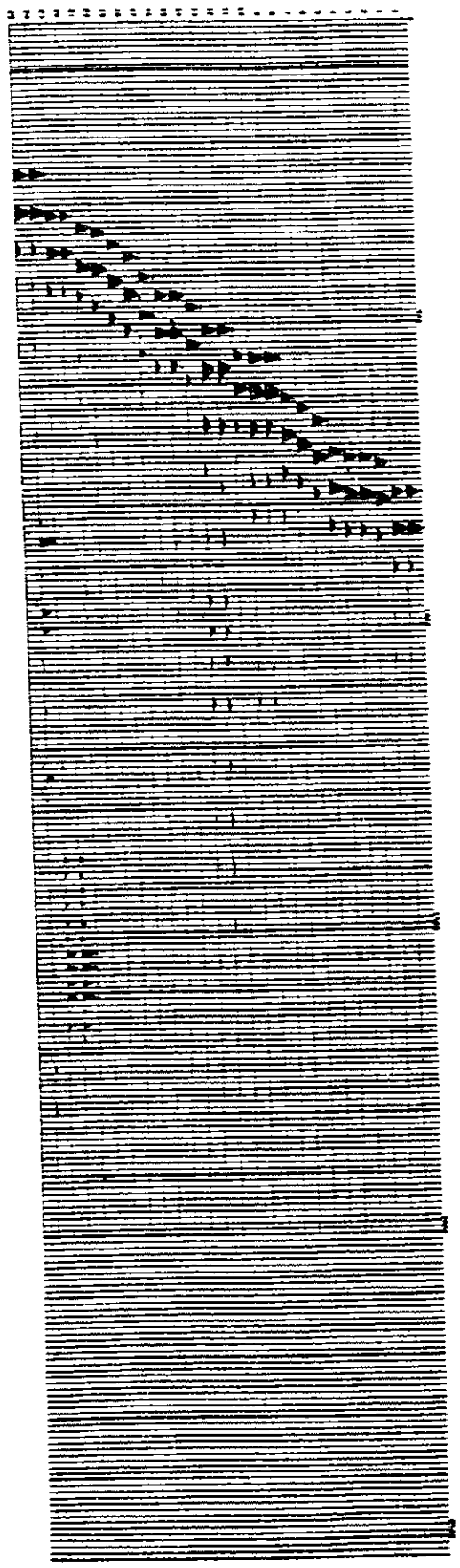


FIGURE 2b

CROSS-CORRELATION OF CHECKSHOT
(PT26 - PT38), NORMALIZED

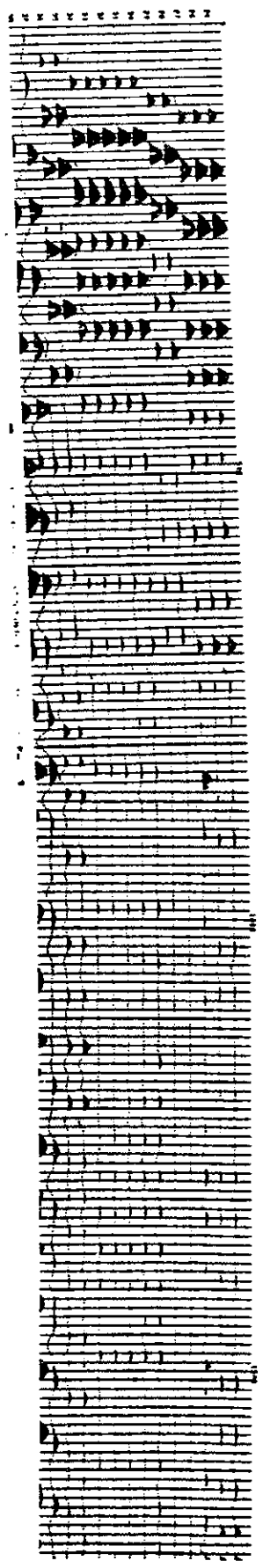


FIGURE 3a

NORMALIZED RAW DATA OF
UPHOLE (DYNAMITE) SURVEY
(40 Hz Geophone)

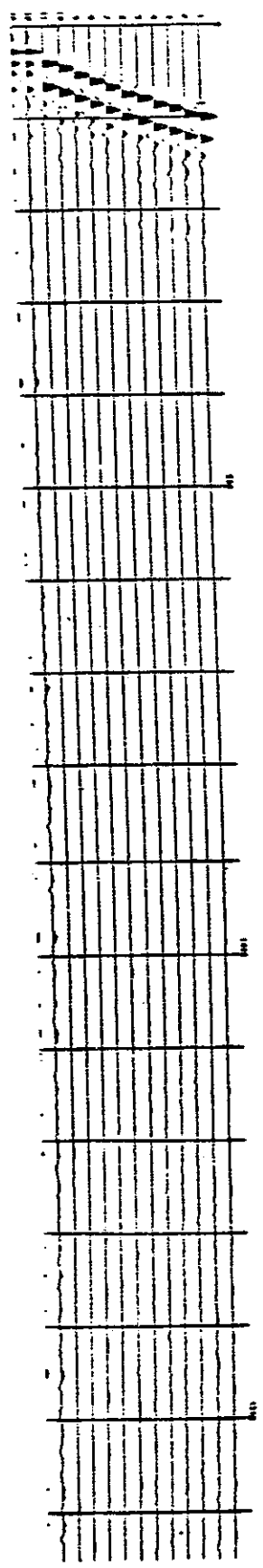


FIGURE 3b

NORMALIZED RAW DATA OF
UPHOLE (DYNAMITE) SURVEY
(14 Hz Geophone)

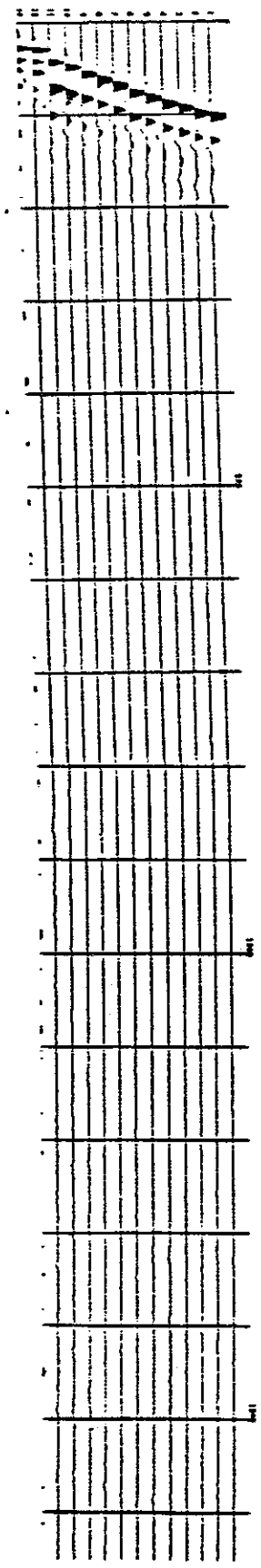


FIGURE 3c

NORMALIZED RAW DATA OF
UPHOLE (DYNAMITE) SURVEY
(40 Hz Geophone)

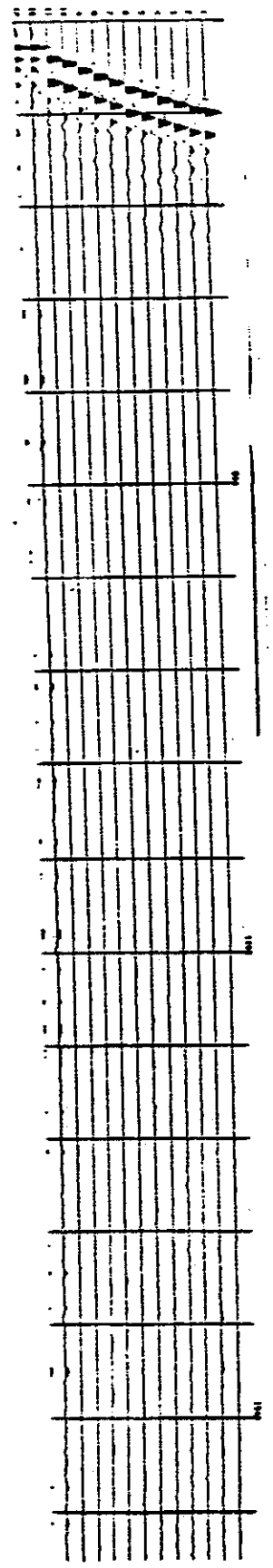


FIGURE 4a

CROSS-CORRELATION OF UPHOLE (DYNAMITE) SURVEY AND NORMALIZED (40 Hz Geophones)

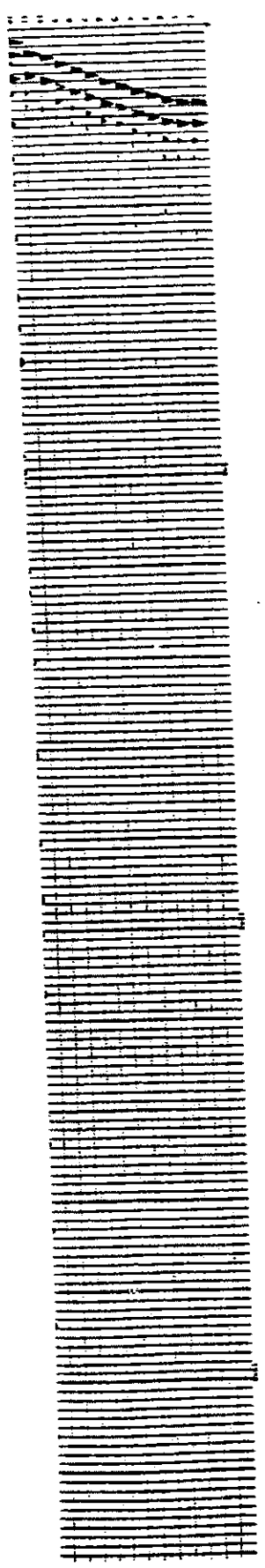


FIGURE 4b

CROSS-CORRELATION OF UPHOLE (DYNAMITE) SURVEY AND NORMALIZED (14 Hz Geophones)

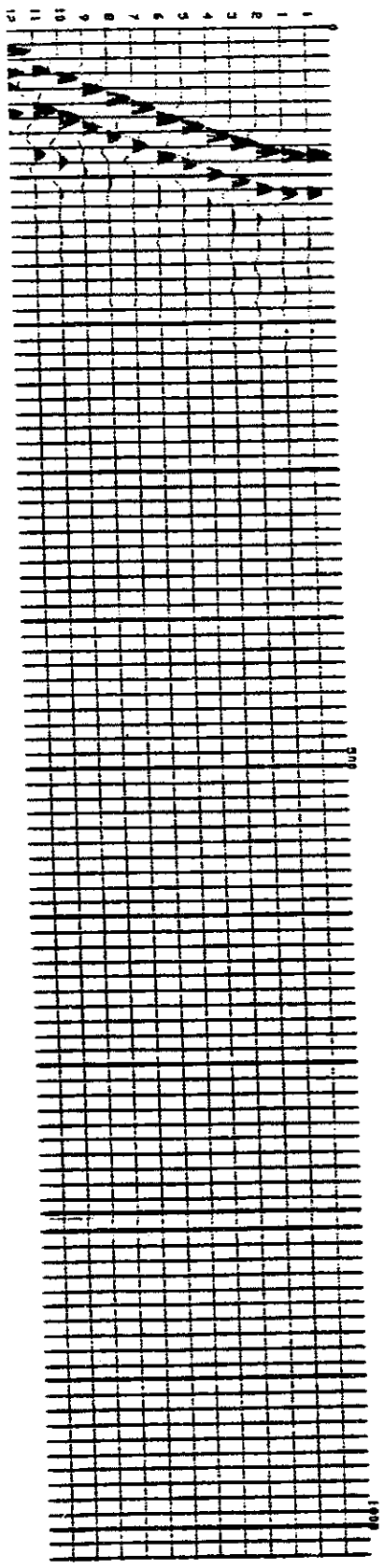


FIGURE 4c

CROSS-CORRELATION OF UPHOLE (DYNAMITE) DATA AND NORMALIZED (40 Hz Geophones)

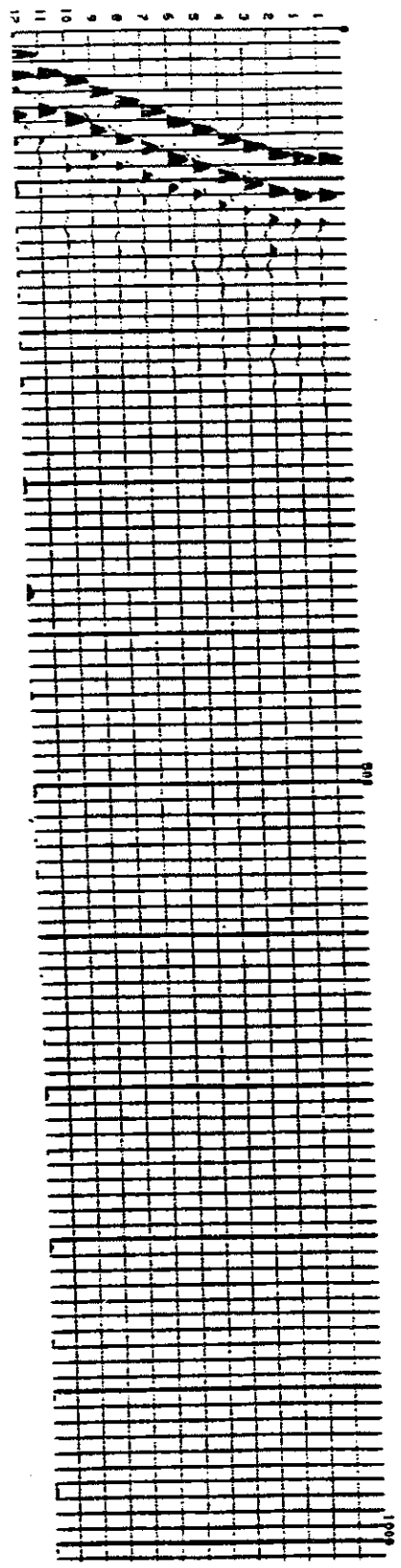
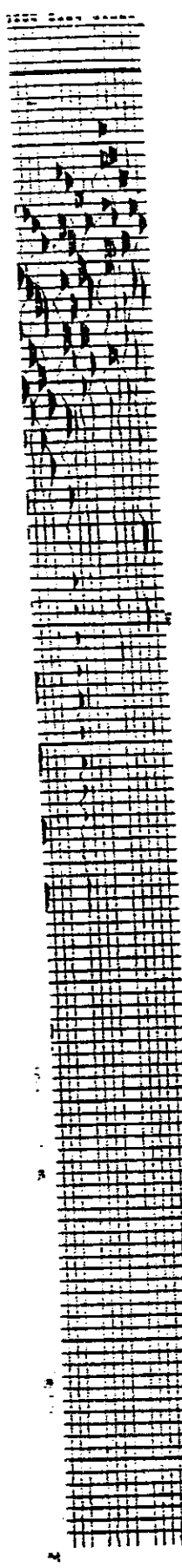
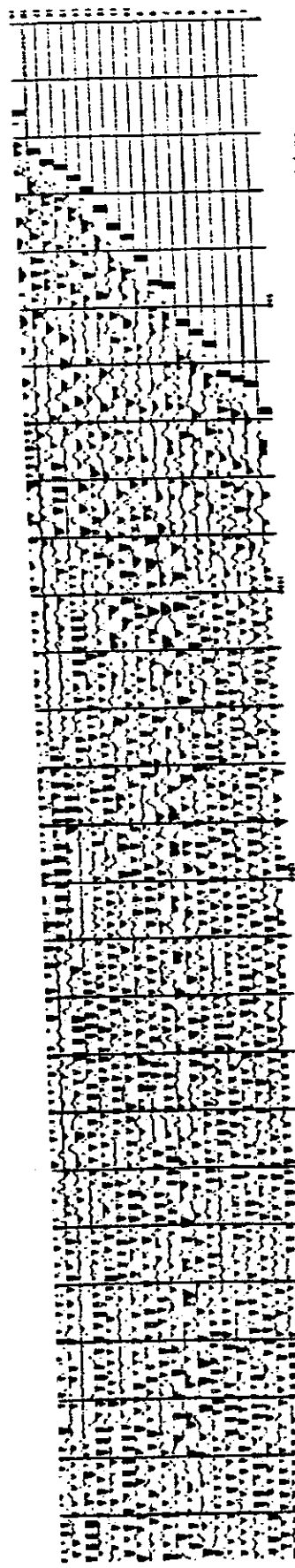


FIGURE 5



NORMALIZED
RAW DATA OF
LATERAL
STEP OUT
SURVEY

FIGURE 6



SHAPING
DECONVOLUTION

FIGURE 7

FK FILTER

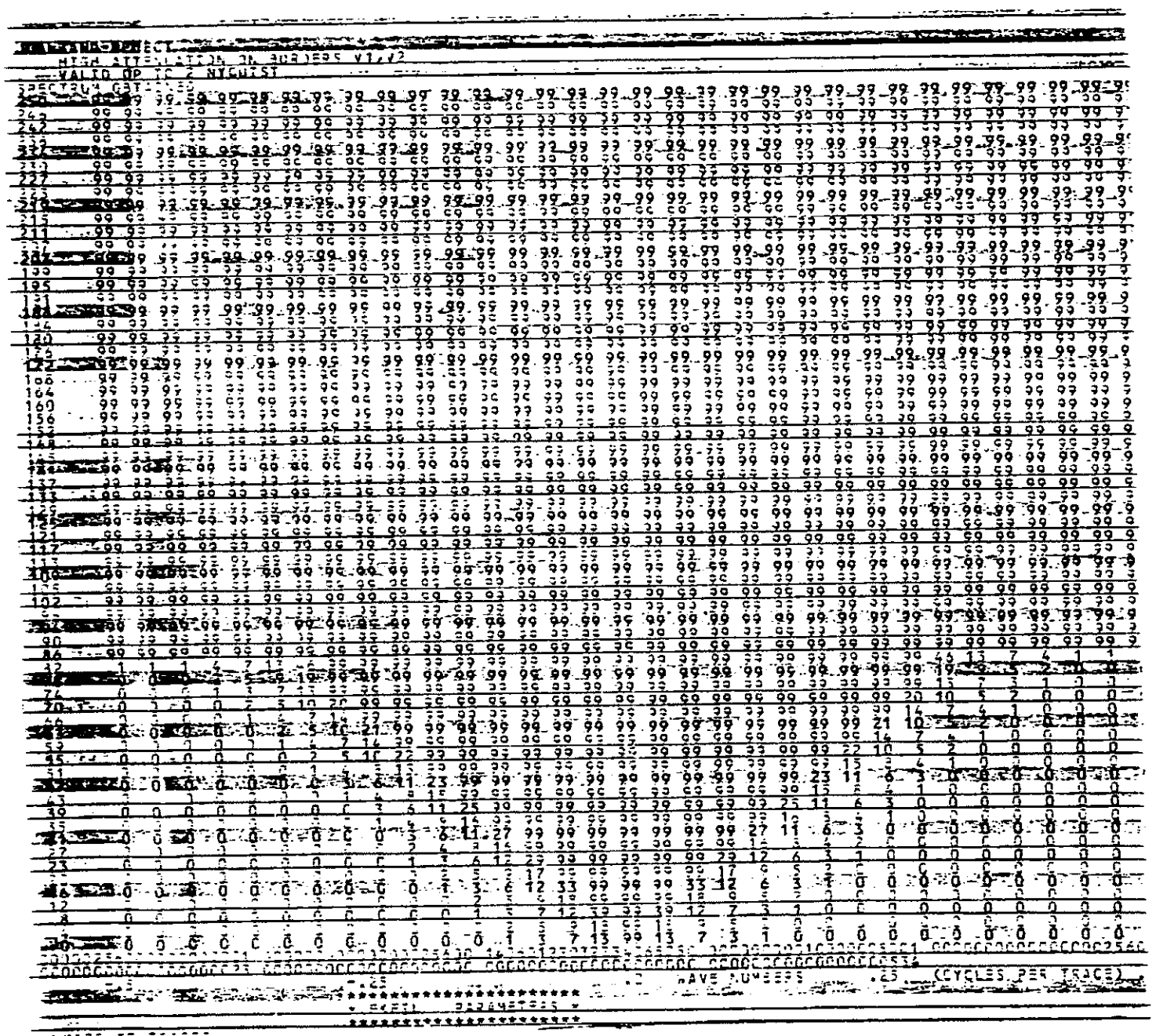
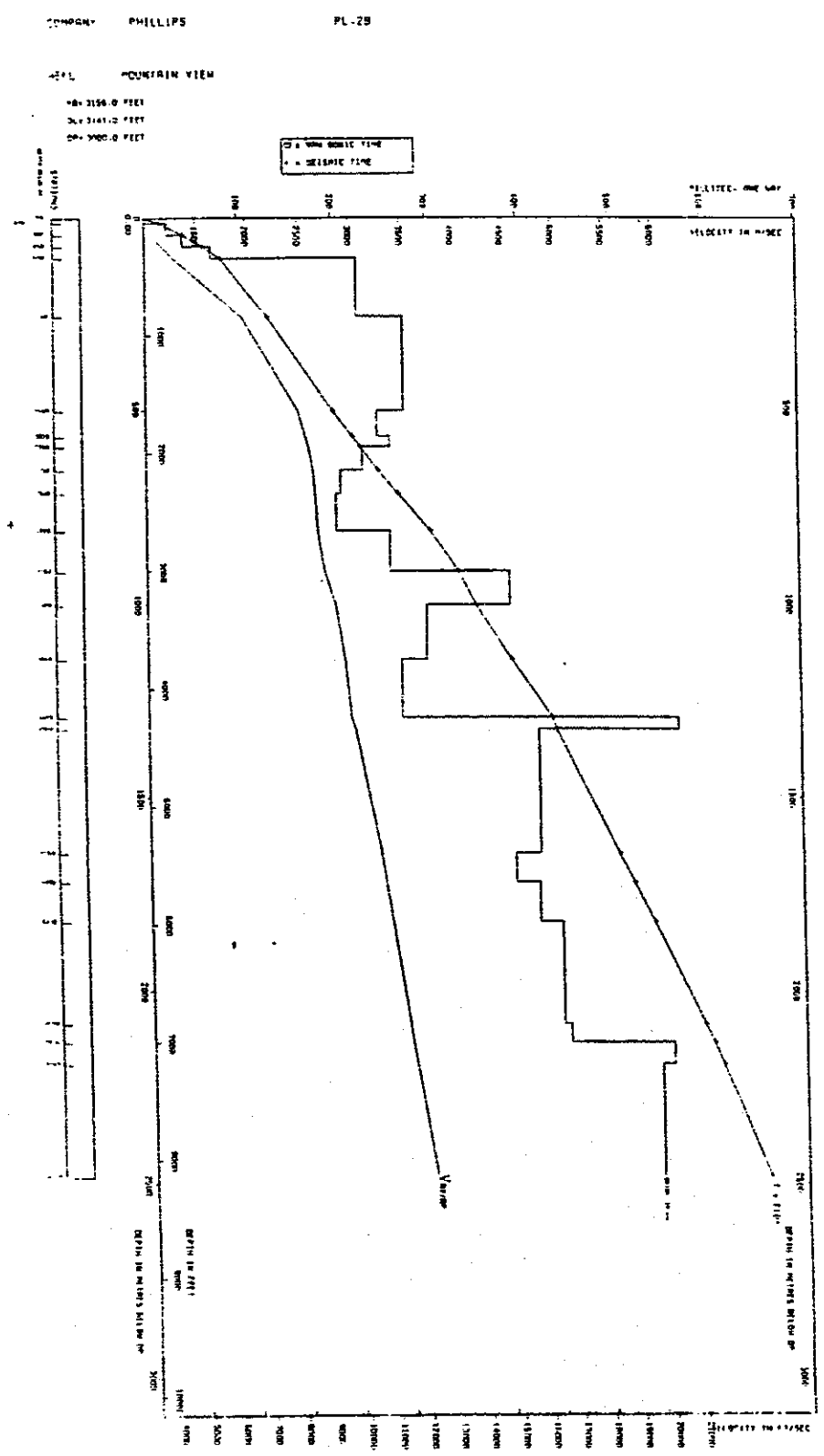


FIGURE 8

ABSOLUTE VERTICAL TIME AND INTERVAL VELOCITIES VS. DEPTH



LIST OF SYMBOLS

for

Velocity Survey Computation Forms

DP:	Datum plane elevation (origin of times)
R:	Rotary table or kelly bushing elevation (origin of depths)
GL:	Ground level elevation
H0-H1-H2:	Thicknesses of weathering zones
V0-V1-V2:	Velocities of weathering zones
VC:	Correction velocity used from GL to DP
C:	Time difference from GL to DP (using VC)
DG:	Downhole station depth below R
DGDP:	Downhole station depth below DP
N:	Field record number
SP:	Source position number
SPE:	Source position elevation
DS:	Depth of bottom of source below GL
D:	Source offset from the well
H:	Vertical depth from source to downhole station
COS:	Cosine of angle between vertical and source location
T:	First break time pick from signature probe to downhole station
T2:	Vertical time from signature probe to downhole station
TI:	Time correction from signature probe to DP
T3:	Vertical seismic time from DP to downhole station
ST:	Sonic time
DFT:	Drift (T3 - ST)
IV:	Interval velocity between stations
AV:	Average velocity from DP
T3M:	Average vertical seismic time
DM:	Average drift (T3M - ST)

PHILLIPS
SEPTEMBER 20, 1982

MOUNTAIN VIEW

VELOCITY SURVEY COMPUTATION FORMS
IN DENVER - U.S.A.

PARAMETERS

DP =	3000.0
R =	3156.0
GL =	3141.0
MO =	0.0
VO =	6714.0
M1 =	0.0
V1 =	0.0
M2 =	0.0
V2 =	0.0
VC =	6714.0

LENGTH UNIT = FEET

UNCORRECTED TIMES TO GL = UCT
UCT = T3 + C

C = 21.0

DGR	DGDP	N	SP	SPE	DS	D	H	COS	T	T2	TI	T3	ST	DFT	IV	AV	T3M	D
															6418			
1000	844	25	25	3141.0	0	42	985	.9991	152.7	152.6	-21.0	131.6						
1000	844	24	24	3141.0	0	42	985	.9991	152.5	152.4	-21.0	131.4			11561	6418	131.5	
1800	1644	23	23	3141.0	0	42	1785	.9997	221.9	221.8	-21.0	200.8						
1800	1644	22	22	3141.0	0	42	1785	.9997	221.7	221.6	-21.0	200.6			10697	8191	200.7	
2015	1859	21	21	3141.0	0	42	2000	.9998	241.9	241.8	-21.0	220.8			11111	8419	220.8	
2105	1949	20	20	3141.0	0	42	2090	.9998	250.0	249.9	-21.0	228.9			10209	8515	228.9	
2300	2144	19	19	3141.0	0	42	2255	.9998	269.0	269.0	-21.0	248.0			9524	8645	245.0	
2500	2344	18	18	3141.0	0	42	2485	.9999	290.0	290.0	-21.0	269.0			9377	8714	269.0	
2815	2660	17	17	3141.0	0	42	2801	.9999	323.7	323.7	-21.0	302.7			11033	8788	302.7	
3164	3008	16	16	3141.0	0	42	3149	.9999	356.9	356.9	-21.0	333.9						
3164	3008	15	15	3141.0	0	42	3149	.9999	355.3	355.3	-21.0	334.3			14974	9003	334.1	
3450	3294	14	14	3141.0	0	42	3435	.9999	374.2	374.2	-21.0	353.2			12234	9326	353.2	
3910	3754	13	13	3141.0	0	42	3895	.9999	411.9	411.9	-21.0	390.9						
3910	3754	12	12	3141.0	0	42	3895	.9999	411.8	411.8	-21.0	390.8			11422	9606	390.8	
4400	4244	11	11	3141.0	0	42	4385	1.0000	454.7	454.7	-21.0	433.7			20408	9786	433.7	
4500	4344	10	10	3141.0	0	42	4485	1.0000	459.8	459.8	-21.0	438.8						
4500	4344	9	9	3141.0	0	42	4485	1.0000	459.4	459.4	-21.0	438.4			15601	9904	438.6	
5550	5394	8	8	3141.0	0	42	5535	1.0000	525.8	525.8	-21.0	504.8			15060	10685	504.8	
5800	5644	7	7	3141.0	0	42	5785	1.0000	542.4	542.4	-21.0	521.4			15802	10825	521.4	
6135	5979	6	6	3141.0	0	42	6120	1.0000	563.6	563.6	-21.0	542.6			16539	11019	542.6	
7000	6844	5	5	3141.0	0	42	6985	1.0000	615.9	615.9	-21.0	594.9			16774	11504	594.9	
7156	7000	4	4	3141.0	0	42	7141	1.0000	625.2	625.2	-21.0	604.2						
7156	7000	3	3	3141.0	0	42	7141	1.0000	625.5	625.5	-21.0	604.5			20108	11586	604.2	
7343	7187	2	2	3141.0	0	42	7328	1.0000	634.5	634.5	-21.0	613.5			19752	11715	613.5	
8300	8144	1	1	3141.0	0	42	8285	1.0000	683.0	683.0	-21.0	662.0				12302	662.0	

T3M = AVERAGE VERTICAL TIME DM = AVERAGE DRIFT * DOUBTFUL VALUE / CANCELLED VALUE

LIST OF SYMBOLS

for

Listing of Results

DELTA T:	Sampling interval (milliseconds one-way time)
TAU:	Calculation interval (milliseconds one-way time)
H:	Depth difference from KB to GL
S:	CVL depth unit conversion coefficient
ZO:	Depth below GL of first sample of CVL
THO:	Time corresponding to ZO
DFT:	Drift (seismic time minus Sonic time)
DT DFT:	Difference in drift
ZKB:	Depth below KB (used for drift calculation)
DZ:	Difference in ZKB
AST:	Adjusted Sonic time (after drift correction)
DTA:	Difference in AST
DTMIN:	Minimum travel time found on Sonic log
T:	Time below DP
DKB:	Depth below KB
DDP:	Depth below DP
IV:	Interval velocity between samples
K:	Reflection coefficient
VAV:	Average velocity from DP
VRMS:	RMS velocity from DP
DT:	Theoretical normal moveout for seismic spread of length x
ALPHA:	Attenuation coefficient
DENS:	Bulk density (grams/cc)
T3M:	Average vertical seismic time
DM:	Drift (T3M - ST)
AVST:	Adjusted vertical Sonic time
E:	Final difference in time (T3M - AVST)
AV:	Average velocity from DP

LISTING OF RESULTS

WELL	MOUNTAIN VIEW
COMPANY	PHILLIPS
COUNTRY	U.S. OF A.
X	SECTION 10
Y	T17S,R15E
KB	3156
GL	3141
DP	GL (3141)

COMPUTED IN DENVER-U.S.A.

UNITS
-DEPTH = FEET
-VELOCITY = FEET/SECOND
-TIME = MILLISECONDS (ONE WAY)

CALCULATION

DP =GL (3141)

VELOCITY BETWEEN THE SURFACE AND THE BEGINNING OF THE CVL , VS= 6900.

VALUES OF PARAMETERS

DELTA T = 1.0
TAU = 1.0
H = -15.0
S =1.0000
ZO = 21.9
THO = 1.0

CALCULATION BY FORMULA K= (V1*D1 - V2*D2) / (V1*D1 + V2*D2)

CALIBRATION
CORRECTION FORMULAE

CALIBRATION
CORRECTION FORMULAE

EITHER ATT =TT + CSTE WHERE TT = SAMPLED TRANSIT TIME
AND CSTE = (DT DFT)*1000 / DZ

OR ATT = (TT-DTMIN)*CK + DTMIN WHERE CK = (DTA*1000-DTMIN*DZ)/(DTS*1000-DTMIN*DZ)

DFT	DT DFT	ZKB	DZ	AST	DTA	ST	DTS	PERCENTAGE DTMIN	PERCENTAGE CK	CSTE
0.0		1070.0		153.0		153.0				
	-36.5		950.0		94.1		130.6	50.00	.56066	
-36.5		2020.0		247.1		283.6				
	-34.5		470.0		45.3		79.8	50.00	.38754	
-71.0		2490.0		292.4		363.4				
	-34.0		640.0		63.5		97.5	50.00	.48107	
-105.0		3130.0		355.9		460.9				
	-98.0		2535.0		181.3		279.3	50.00	.35738	
-203.0		5665.0		537.2		740.2				
	-8.0		470.0		30.5		38.5	50.00	.46560	
-211.0		6135.3		567.7		776.7				
	-5.3		2165.0		119.4		124.7	50.00	.67859	
-216.3		8300.0		687.1		903.4				
	0.0		11.7		.6		.6	50.00	1.00000	
-216.3		8311.7		687.7		904.0				

ATT IS ADJUSTED TRANSIT TIME

CSTE AND DTMIN ARE EXPRESSED IN MICROSECONDS/ FEET

T	DXB	DDP	IV	K	VAV	VRMS	DT FOR X = 0.	0.	0.	ALPHA	DENS
1.0	21.9	6.9	6900.0	.001	6900.0	6900.0	0.0	0.0	0.0	1.000	2.47
2.0	28.8	13.8	6890.0	-.001	6895.0	6895.0	0.0	0.0	0.0	1.000	2.47
3.0	35.7	20.7	6900.0	.001	6896.7	6896.7	0.0	0.0	0.0	1.000	2.47
4.0	42.6	27.6	6890.0	-.001	6895.0	6895.0	0.0	0.0	0.0	1.000	2.47
5.0	49.5	34.5	6900.0	.001	6896.0	6896.0	0.0	0.0	0.0	1.000	2.47
6.0	56.4	41.4	6890.0	-.001	6895.0	6895.0	0.0	0.0	0.0	1.000	2.47
7.0	63.3	48.3	6900.0	.001	6895.7	6895.7	0.0	0.0	0.0	1.000	2.47
8.0	70.2	55.2	6890.0	-.001	6895.0	6895.0	0.0	0.0	0.0	1.000	2.47
9.0	77.1	62.1	6900.0	.001	6895.6	6895.6	0.0	0.0	0.0	1.000	2.47
10.0	84.0	69.0	6890.0	-.001	6895.0	6895.0	0.0	0.0	0.0	1.000	2.47
11.0	90.9	75.9	6900.0	0.000	6895.5	6895.5	0.0	0.0	0.0	1.000	2.47
12.0	97.8	82.8	6900.0	.001	6895.8	6895.8	0.0	0.0	0.0	1.000	2.47
13.0	104.6	89.6	6900.0	-.001	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
14.0	111.5	96.5	6900.0	.001	6895.7	6895.7	0.0	0.0	0.0	1.000	2.47
15.0	118.4	103.4	6890.0	-.001	6895.3	6895.3	0.0	0.0	0.0	1.000	2.47
16.0	125.3	110.3	6900.0	.001	6895.6	6895.6	0.0	0.0	0.0	1.000	2.47
17.0	132.2	117.2	6890.0	-.001	6895.3	6895.3	0.0	0.0	0.0	1.000	2.47
18.0	139.1	124.1	6900.0	.001	6895.6	6895.6	0.0	0.0	0.0	1.000	2.47
19.0	146.0	131.0	6890.0	-.001	6895.3	6895.3	0.0	0.0	0.0	1.000	2.47
20.0	152.9	137.9	6900.0	.001	6895.5	6895.5	0.0	0.0	0.0	1.000	2.47

T	DXB	DDP	IV	K	VAV	VAMS	DT FOR X = 0.	0.	ALPHA	DENS
21.0	159.8	144.8	690.0	-.001	689.2	689.2	0.0	0.0	1.000	2.47
22.0	166.7	151.7	690.0	.001	689.5	689.3	0.0	0.0	1.000	2.47
23.0	173.6	158.6	690.0	-.001	689.2	689.2	0.0	0.0	1.000	2.47
24.0	180.5	165.5	690.0	-.000	689.4	689.4	0.0	0.0	1.000	2.47
25.0	187.4	172.4	690.0	.001	689.6	689.6	0.0	0.0	1.000	2.47
26.0	194.3	179.3	690.0	-.001	689.4	689.4	0.0	0.0	1.000	2.47
27.0	201.2	186.2	690.0	.001	689.6	689.6	0.0	0.0	1.000	2.47
28.0	208.1	193.1	690.0	-.001	689.4	689.4	0.0	0.0	1.000	2.47
29.0	215.0	200.0	690.0	.001	689.5	689.5	0.0	0.0	1.000	2.47
30.0	221.9	206.9	690.0	-.001	689.3	689.3	0.0	0.0	1.000	2.47
31.0	228.8	213.8	690.0	.001	689.5	689.5	0.0	0.0	1.000	2.47
32.0	235.7	220.7	690.0	-.001	689.3	689.3	0.0	0.0	1.000	2.47
33.0	242.6	227.6	690.0	.001	689.5	689.5	0.0	0.0	1.000	2.47
34.0	249.4	234.4	690.0	-.001	689.3	689.3	0.0	0.0	1.000	2.47
35.0	256.3	241.3	690.0	.000	689.4	689.4	0.0	0.0	1.000	2.47
36.0	263.2	248.2	690.0	.001	689.6	689.6	0.0	0.0	1.000	2.47
37.0	270.1	255.1	690.0	-.001	689.4	689.4	0.0	0.0	1.000	2.47
38.0	277.0	262.0	690.0	.001	689.5	689.5	0.0	0.0	1.000	2.47
39.0	283.9	268.9	690.0	-.001	689.4	689.4	0.0	0.0	1.000	2.47
40.0	290.8	275.8	690.0	.001	689.5	689.5	0.0	0.0	1.000	2.47

T	UKB	DDP	IV	K	VAV	VRMS	0.	DT FOR X = 0.	0.	ALPHA	DENS
41.0	297.7	282.7	6890.0	-.001	6895.4	6895.4	0.0	0.0	0.0	1.030	2.47
42.0	304.6	289.6	6900.0	.001	6895.5	6895.5	0.0	0.0	0.0	1.000	2.47
43.0	311.5	296.5	6890.0	-.001	6895.3	6895.4	0.0	0.0	0.0	1.000	2.47
44.0	318.4	303.4	6900.0	.001	6895.5	6895.5	0.0	0.0	0.0	1.000	2.47
45.0	325.3	310.3	6890.0	-.001	6895.3	6895.3	0.0	0.0	0.0	1.000	2.47
46.0	332.2	317.2	6900.0	.001	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
47.0	339.1	324.1	6890.0	-.001	6895.3	6895.3	0.0	0.0	0.0	1.000	2.47
48.0	346.0	331.0	6900.0	0.000	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
49.0	352.9	337.9	6900.0	.001	6895.5	6895.5	0.0	0.0	0.0	1.000	2.47
50.0	359.8	344.8	6890.0	-.001	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
51.0	366.7	351.7	6900.0	.001	6895.5	6895.5	0.0	0.0	0.0	1.000	2.47
52.0	373.6	358.6	6890.0	-.001	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
53.0	380.5	365.5	6900.0	.001	6895.5	6895.5	0.0	0.0	0.0	1.000	2.47
54.0	387.4	372.4	6890.0	-.001	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
55.0	394.3	379.3	6900.0	.001	6895.5	6895.5	0.0	0.0	0.0	1.000	2.47
56.0	401.1	386.1	6890.0	-.001	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
57.0	408.0	393.0	6900.0	.001	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
58.0	414.9	399.9	6890.0	-.001	6895.3	6895.3	0.0	0.0	0.0	1.000	2.47
59.0	421.8	406.9	6900.0	0.000	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
60.0	428.7	413.7	6900.0	.001	6895.5	6895.5	0.0	0.0	0.0	1.000	2.47

T	DKB	DUP	IV	K	VAV	VRMS	DT FOR X = 0.	0.	0.	ALPHA	DENS
61.0	435.6	420.6	6890.0	-.001	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
62.0	442.5	427.5	6900.0	.001	6895.5	6895.5	0.0	0.0	0.0	1.000	2.47
63.0	449.4	434.4	6890.0	-.001	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
64.0	456.3	441.3	6900.0	.001	6895.5	6895.5	0.0	0.0	0.0	1.000	2.47
65.0	463.2	448.2	6890.0	-.001	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
66.0	470.1	455.1	6900.0	.001	6895.5	6895.5	0.0	0.0	0.0	1.000	2.47
67.0	477.0	462.0	6890.0	-.001	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
68.0	483.9	468.9	6900.0	.001	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
69.0	490.8	475.8	6890.0	-.001	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
70.0	497.7	482.7	6900.0	0.000	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
71.0	504.6	489.6	6900.0	.001	6895.5	6895.5	0.0	0.0	0.0	1.000	2.47
72.0	511.5	496.5	6890.0	-.001	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
73.0	518.4	503.4	6900.0	.001	6895.5	6895.5	0.0	0.0	0.0	1.000	2.47
74.0	525.3	510.3	6890.0	-.001	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
75.0	532.2	517.2	6900.0	.001	6895.5	6895.5	0.0	0.0	0.0	1.000	2.47
76.0	539.1	524.1	6890.0	-.001	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
77.0	546.0	531.0	6900.0	.001	6895.5	6895.5	0.0	0.0	0.0	1.000	2.47
78.0	552.8	537.8	6890.0	-.001	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
79.0	559.7	544.7	6900.0	.001	6895.4	6895.4	0.0	0.0	0.0	1.000	2.47
80.0	566.6	551.6	6890.0	-.001	6895.4	6895.4	0.0	0.0	0.0		

T	DKB	DDP	IV	K	VAV	VRMS	Q.	Q.	ALPHA	DENS
							DT FOR X =			
81.0	573.5	558.5	690.0	.001	6895.4	6895.4	0.0	0.0	1.000	2.47
82.0	580.4	565.4	690.0	-.001	6895.4	6895.4	0.0	0.0	1.000	2.47
83.0	587.3	572.3	690.0	0.000	6895.4	6895.4	0.0	0.0	1.000	2.47
84.0	594.2	579.2	690.0	.001	6895.5	6895.5	0.0	0.0	1.000	2.47
85.0	601.1	586.1	690.0	-.001	6895.4	6895.4	0.0	0.0	1.000	2.47
86.0	608.0	593.0	690.0	.001	6895.5	6895.5	0.0	0.0	1.000	2.47
87.0	614.9	599.9	690.0	-.001	6895.4	6895.4	0.0	0.0	1.000	2.47
88.0	621.8	606.8	690.0	.001	6895.5	6895.5	0.0	0.0	1.000	2.47
89.0	628.7	613.7	690.0	-.001	6895.4	6895.4	0.0	0.0	1.000	2.47
90.0	635.6	620.6	690.0	.001	6895.4	6895.4	0.0	0.0	1.000	2.47
91.0	642.5	627.5	690.0	-.001	6895.4	6895.4	0.0	0.0	1.000	2.47
92.0	649.4	634.4	690.0	.001	6895.4	6895.4	0.0	0.0	1.000	2.47
93.0	656.3	641.3	690.0	-.001	6895.4	6895.4	0.0	0.0	1.000	2.47
94.0	663.2	648.2	690.0	-.000	6895.4	6895.4	0.0	0.0	1.000	2.47
95.0	670.1	655.1	690.0	.001	6895.5	6895.5	0.0	0.0	1.000	2.47
96.0	677.0	662.0	690.0	-.001	6895.4	6895.4	0.0	0.0	1.000	2.47
97.0	683.9	668.9	690.0	.001	6895.5	6895.5	0.0	0.0	1.000	2.47
98.0	690.8	675.8	690.0	-.001	6895.4	6895.4	0.0	0.0	1.000	2.47
99.0	697.7	682.7	690.0	.001	6895.5	6895.5	0.0	0.0	1.000	2.47
100.0	704.5	689.5	690.0	-.001	6895.4	6895.4	0.0	0.0	1.000	2.47

T	DKB	DOP	IV	K	VAV	VRMS	DT FOR X = 0.	0.	0.	ALPHA	DENS
			6900.0							1.000	2.47
101.0	711.4	696.4		.001	6895.4	6895.4	0.0	0.0	0.0		
			6890.0							1.000	2.47
102.0	718.3	703.3		-.001	6895.4	6895.4	0.0	0.0	0.0		
			6900.0							1.000	2.47
103.0	725.2	710.2		.001	6895.4	6895.4	0.0	0.0	0.0		
			6890.0							1.000	2.47
104.0	732.1	717.1		-.001	6895.4	6895.4	0.0	0.0	0.0		
			6900.0							1.000	2.47
105.0	739.0	724.0		.000	6895.4	6895.4	0.0	0.0	0.0		
			6900.0							1.000	2.47
106.0	745.9	730.9		.001	6895.5	6895.5	0.0	0.0	0.0		
			6890.0							1.000	2.47
107.0	752.8	737.8		-.001	6895.4	6895.4	0.0	0.0	0.0		
			6900.0							1.000	2.47
108.0	759.7	744.7		.001	6895.5	6895.5	0.0	0.0	0.0		
			6890.0							1.000	2.47
109.0	766.6	751.6		-.001	6895.4	6895.4	0.0	0.0	0.0		
			6900.0							1.000	2.47
110.0	773.5	758.5		.001	6895.5	6895.5	0.0	0.0	0.0		
			6890.0							1.000	2.47
111.0	780.4	765.4		-.001	6895.4	6895.4	0.0	0.0	0.0		
			6900.0							1.000	2.47
112.0	787.3	772.3		.001	6895.4	6895.4	0.0	0.0	0.0		
			6890.0							1.000	2.47
113.0	794.2	779.2		-.001	6895.4	6895.4	0.0	0.0	0.0		
			6900.0							1.000	2.47
114.0	801.1	786.1		.001	6895.4	6895.4	0.0	0.0	0.0		
			6890.0							1.000	2.47
115.0	808.0	793.0		-.001	6895.4	6895.4	0.0	0.0	0.0		
			6900.0							1.000	2.47
116.0	814.9	799.9		.001	6895.4	6895.4	0.0	0.0	0.0		
			6890.0							1.000	2.47
117.0	821.8	806.8		-.001	6895.4	6895.4	0.0	0.0	0.0		
			6900.0							1.000	2.47
118.0	828.7	813.7		0.000	6895.4	6895.4	0.0	0.0	0.0		
			6900.0							1.000	2.47
119.0	835.6	820.6		.001	6895.5	6895.5	0.0	0.0	0.0		
			6890.0							1.000	2.47
120.0	842.5	827.5		-.001	6895.4	6895.4	0.0	0.0	0.0		

DT FOR X =	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
ALPHA	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
DENS	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47	2.47

I	DXB	DDP	IV	K	VAV	VRMS
121.0	649.4	834.3	6900.0	.001	6895.5	6895.5
122.0	656.2	841.2	6900.0	-.001	6895.4	6895.4
123.0	863.1	848.1	6900.0	.001	6895.4	6895.4
124.0	870.0	855.0	6900.0	-.001	6895.4	6895.4
125.0	876.9	861.9	6900.0	.001	6895.4	6895.4
126.0	883.8	868.8	6900.0	-.001	6895.4	6895.4
127.0	890.7	875.7	6900.0	.001	6895.4	6895.4
128.0	897.6	882.6	6900.0	-.001	6895.4	6895.4
129.0	904.5	889.5	6900.0	-.000	6895.4	6895.4
130.0	911.4	896.4	6900.0	.001	6895.5	6895.5
131.0	918.3	903.3	6900.0	-.001	6895.4	6895.4
132.0	925.2	910.2	6900.0	.001	6895.5	6895.5
133.0	932.1	917.1	6900.0	-.001	6895.4	6895.4
134.0	939.0	924.0	6900.0	.001	6895.4	6895.4
135.0	945.9	930.9	6900.0	-.001	6895.4	6895.4
136.0	952.8	937.8	6900.0	.001	6895.4	6895.4
137.0	959.7	944.7	6900.0	-.001	6895.4	6895.4
138.0	966.6	951.6	6900.0	.001	6895.4	6895.4
139.0	973.5	958.5	6900.0	-.001	6895.4	6895.4
140.0	980.4	965.4	6900.0	.001	6895.4	6895.4

T	DKO	DDP	IV	K	VAV	VRMS	RT FOR X = 0.	0.	ALPHA	DENS
141.0	987.2	972.3	690.0	-.001	689.4	689.4	0.0	0.0	1.000	2.47
142.0	994.2	979.2	690.0	.000	689.4	689.4	0.0	0.0	1.000	2.47
143.0	1001.1	986.1	690.0	.001	689.5	689.5	0.0	0.0	1.000	2.47
144.0	1007.9	992.9	690.0	-.001	689.4	689.4	0.0	0.0	1.000	2.47
145.0	1014.8	999.8	690.0	.001	689.4	689.5	0.0	0.0	1.000	2.47
146.0	1021.7	1006.7	690.0	-.001	689.4	689.4	0.0	0.0	1.000	2.47
147.0	1028.6	1013.6	690.0	.001	689.4	689.4	0.0	0.0	1.000	2.47
148.0	1035.5	1020.5	690.0	-.001	689.4	689.4	0.0	0.0	1.000	2.47
149.0	1042.4	1027.4	690.0	.001	689.4	689.4	0.0	0.0	1.000	2.47
150.0	1049.3	1034.3	690.0	-.001	689.4	689.4	0.0	0.0	1.000	2.47
151.0	1056.2	1041.2	690.0	.001	689.4	689.4	0.0	0.0	1.000	2.47
152.0	1063.1	1048.1	690.0	-.001	689.4	689.4	0.0	0.0	1.000	2.47
153.0	1070.0	1055.0	690.0	0.000	689.4	689.4	0.0	0.0	1.000	2.47
154.0	1079.9	1064.9	690.0	-.028	691.4	691.8	0.0	0.0	.999	2.47
155.0	1090.3	1075.3	1043.4	-.000	693.5	694.3	0.0	0.0	-.999	2.47
156.0	1100.7	1085.7	1043.9	.023	695.9	697.2	0.0	0.0	.999	2.47
157.0	1111.0	1095.7	998.2	.021	697.2	699.5	0.0	0.0	.996	2.44
158.0	1120.4	1105.4	967.8	-.017	699.3	701.8	0.0	0.0	.998	2.48
159.0	1130.3	1115.3	986.7	.036	701.3	704.2	0.0	0.0	.998	2.47
160.0	1140.1	1125.1	979.1	-.013	703.7	706.8	0.0	0.0	.998	2.47

T	DKB	DDP	IV	K	VAV	VRMS	DT FOR X 0.	0.	0.	ALPHA	DENS
161.0	1150.3	1135.3	10186.4	.016	7051.3	7084.4	0.0	0.0	0.0	.998	2.44
162.0	1160.3	1145.3	10070.3	.028	7069.9	7106.7	0.0	0.0	0.0	.997	2.39
163.0	1170.2	1155.2	9847.7	.017	7087.0	7126.7	0.0	0.0	0.0	.997	2.31
164.0	1180.1	1165.1	9395.6	-.008	7104.1	7146.9	0.0	0.0	0.0	.996	2.22
165.0	1190.2	1175.2	10140.7	-.000	7122.5	7168.8	0.0	0.0	0.0	.996	2.20
166.0	1200.3	1185.3	10063.1	.010	7140.2	7189.7	0.0	0.0	0.0	.996	2.22
167.0	1210.4	1195.4	10142.0	.038	7158.2	7211.0	0.0	0.0	0.0	.996	2.16
168.0	1220.5	1205.5	10070.5	-.001	7175.5	7231.4	0.0	0.0	0.0	.996	2.14
169.0	1230.7	1215.7	10228.1	-.000	7193.6	7252.7	0.0	0.0	0.0	.996	2.11
170.0	1241.1	1226.1	10341.6	-.000	7212.1	7274.7	0.0	0.0	0.0	.996	2.09
171.0	1251.6	1236.6	10511.5	.012	7231.4	7297.8	0.0	0.0	0.0	.996	2.05
172.0	1261.8	1246.8	10202.5	.006	7248.7	7318.1	0.0	0.0	0.0	.996	2.06
173.0	1272.0	1257.0	10214.4	-.005	7265.8	7338.1	0.0	0.0	0.0	.996	2.04
174.0	1282.4	1267.4	10378.1	-.004	7283.7	7359.1	0.0	0.0	0.0	.996	2.03
175.0	1292.9	1277.9	10501.0	-.002	7302.1	7380.9	0.0	0.0	0.0	.996	2.02
176.0	1303.4	1288.4	10559.9	-.005	7320.6	7402.8	0.0	0.0	0.0	.996	2.02
177.0	1314.1	1299.1	10719.7	.008	7339.8	7425.7	0.0	0.0	0.0	.996	2.01
178.0	1324.7	1309.7	10589.3	-.004	7358.1	7447.3	0.0	0.0	0.0	.996	2.00
179.0	1335.4	1320.4	10684.0	.005	7376.6	7469.2	0.0	0.0	0.0	.996	2.00
180.0	1346.0	1331.0	10557.4	-.004	7394.3	7489.9	0.0	0.0	0.0	.996	2.01

I	OKB	DOP	IV	K	VAV	VRMS	DT FOR X = 0.	0.	0.	ALPHA	DEMS
181.0	1356.5	1341.5	10519.6	-.005	7411.6	7510.0	0.0	0.0	0.0	.996	2.03
182.0	1367.0	1352.0	10523.6	.012	7428.7	7529.9	0.0	0.0	0.0	.996	2.06
183.0	1377.2	1362.2	10219.8	-.013	7443.9	7547.2	0.0	0.0	0.0	.995	2.07
184.0	1387.7	1372.7	10432.5	.000	7460.2	7565.8	0.0	0.0	0.0	.995	2.10
185.0	1397.9	1382.9	10259.3	-.005	7475.3	7582.9	0.0	0.0	0.0	.995	2.15
186.0	1408.1	1393.1	10123.7	-.016	7489.5	7598.9	0.0	0.0	0.0	.995	2.21
187.0	1418.2	1403.2	10175.1	-.023	7503.9	7615.0	0.0	0.0	0.0	.995	2.27
188.0	1428.6	1413.6	10358.9	.012	7519.1	7632.2	0.0	0.0	0.0	.995	2.30
189.0	1438.6	1423.6	9983.6	-.008	7532.1	7646.5	0.0	0.0	0.0	.994	2.34
190.0	1448.5	1433.5	9952.9	-.001	7544.9	7660.5	0.0	0.0	0.0	.994	2.38
191.0	1458.3	1443.3	9800.0	-.010	7556.7	7673.2	0.0	0.0	0.0	.994	2.42
192.0	1468.2	1453.2	9841.8	.003	7566.6	7686.1	0.0	0.0	0.0	.994	2.42
193.0	1478.0	1463.0	9708.2	-.012	7580.1	7698.5	0.0	0.0	0.0	.994	2.45
194.0	1487.9	1472.9	9902.0	-.018	7592.1	7711.5	0.0	0.0	0.0	.994	2.46
195.0	1498.1	1483.1	10238.2	-.005	7605.6	7726.5	0.0	0.0	0.0	.994	2.46
196.0	1508.4	1493.4	10336.9	.020	7619.6	7742.1	0.0	0.0	0.0	.993	2.44
197.0	1518.4	1503.4	10006.7	-.020	7631.7	7755.3	0.0	0.0	0.0	.993	2.47
198.0	1528.8	1513.8	10315.5	.005	7645.2	7770.3	0.0	0.0	0.0	.993	2.47
199.0	1539.0	1524.0	10193.1	-.010	7658.0	7784.4	0.0	0.0	0.0	.993	2.49
200.0	1549.3	1534.3	10314.7	.013	7671.3	7799.1	0.0	0.0	0.0	.993	2.49

I	DKB	DDP	IV	K	VAV	VRMS	Q.	Q.	ALPHA	DENS
							DT FOR X =			
201.0	1559.3	1544.3	10075.0	.024	7683.3	7812.0	0.0	0.0	.993	2.48
202.0	1569.1	1554.1	9659.1	.005	7693.3	7822.6	0.0	0.0	.992	2.45
203.0	1578.7	1563.7	9759.1	-.005	7703.0	7832.7	0.0	0.0	.992	2.44
204.0	1588.5	1573.5	9933.4	-.002	7713.1	7843.3	0.0	0.0	.992	2.43
205.0	1596.3	1583.3	9933.4	-.017	7723.4	7854.2	0.0	0.0	.992	2.44
206.0	1606.5	1593.5	10145.0	-.008	7735.2	7867.0	0.0	0.0	.992	2.45
207.0	1618.7	1603.7	10260.4	.010	7747.4	7880.3	0.0	0.0	.992	2.45
208.0	1628.8	1613.8	10050.6	-.001	7758.5	7892.1	0.0	0.0	.992	2.44
209.0	1638.9	1623.9	10098.0	.007	7769.7	7904.1	0.0	0.0	.992	2.42
210.0	1646.9	1633.9	10043.2	.004	7780.5	7915.7	0.0	0.0	.992	2.44
211.0	1656.6	1643.8	9909.3	-.007	7790.6	7926.3	0.0	0.0	.992	2.43
212.0	1666.9	1653.9	10075.1	-.004	7801.4	7937.8	0.0	0.0	.992	2.44
213.0	1679.0	1664.0	10117.4	-.008	7812.2	7949.5	0.0	0.0	.992	2.45
214.0	1689.2	1674.2	10229.7	-.005	7823.5	7961.6	0.0	0.0	.991	2.46
215.0	1699.5	1684.5	10282.1	-.006	7835.0	7974.0	0.0	0.0	.991	2.46
216.0	1709.9	1694.5	10463.3	-.003	7846.9	7986.9	0.0	0.0	.991	2.46
217.0	1720.4	1705.4	10459.7	.002	7858.9	8000.1	0.0	0.0	.991	2.45
218.0	1730.9	1715.6	10468.1	.014	7870.9	8013.1	0.0	0.0	.991	2.45
219.0	1741.0	1726.0	10102.5	-.012	7881.4	8024.4	0.0	0.0	.991	2.46
220.0	1751.4	1736.4	10392.1	.004	7892.8	8036.7	0.0	0.0	.991	2.46

T	DKB	DDP	IV	K	VAV	VRMS	DT FOR X = 0.	0.	ALPHA	DENS
221.0	1761.8	1746.8	10436.3	-.005	7903.9	8048.6	0.0	0.0	.991	2.45
222.0	1772.2	1757.2	10430.2	.022	7915.3	8060.9	0.0	0.0	.991	2.43
223.0	1782.2	1767.2	10653.9	.010	7924.9	8071.0	0.0	0.0	.990	2.45
224.0	1792.0	1777.0	9781.8	.001	7933.1	8079.4	0.0	0.0	.990	2.45
225.0	1801.8	1786.8	9753.5	.044	7941.2	8087.6	0.0	0.0	.989	2.42
226.0	1810.8	1795.8	9038.6	-.000	7946.1	8092.1	0.0	0.0	.989	2.44
227.0	1819.8	1804.8	8975.0	-.020	7950.6	8096.2	0.0	0.0	.988	2.44
228.0	1829.1	1814.1	9333.6	-.013	7956.7	8102.0	0.0	0.0	.986	2.42
229.0	1838.8	1823.8	9659.7	-.013	7964.1	8109.5	0.0	0.0	.988	2.45
230.0	1848.6	1833.6	9824.6	-.007	7972.2	8117.7	0.0	0.0	.988	2.46
231.0	1858.5	1843.5	9911.9	-.005	7980.6	8126.3	0.0	0.0	.986	2.46
232.0	1868.5	1853.5	10009.1	-.005	7989.4	8135.4	0.0	0.0	.988	2.45
233.0	1878.7	1863.7	10144.9	.005	7958.6	8145.1	0.0	0.0	.986	2.45
234.0	1908.7	1873.7	10056.6	.005	8007.4	8154.2	0.0	0.0	.988	2.46
235.0	1656.8	1883.8	10042.8	-.001	8016.1	8163.1	0.0	0.0	.987	2.48
236.0	1909.1	1894.1	10332.2	-.019	8025.9	8173.5	0.0	0.0	.987	2.46
237.0	1919.4	1904.4	10268.7	.006	8035.4	8183.5	0.0	0.0	.987	2.47
238.0	1929.9	1914.9	10559.3	-.015	8045.9	8194.9	0.0	0.0	.987	2.47
239.0	1940.2	1925.2	10280.8	.013	8055.3	8204.7	0.0	0.0	.987	2.47
240.0	1.950.4	1935.4	10136.6	.007	8064.0	8213.7	0.0	0.0	.987	2.47

T	DKB	DDP	IV	K	VAV	VRMS	Q.	Q.	Q.	ALPHA	DENS
							OT FOR X =				
241.0	1960.0	1945.3	9608.7	-.077	8070.4	8220.0	0.0	0.0	0.0	.966	2.47
242.0	1971.2	1956.2	11262.1	.030	8083.3	8234.6	0.0	0.0	0.0	.960	2.47
243.0	1981.7	1966.7	10569.1	.027	8093.5	8245.5	0.0	0.0	0.0	.959	2.45
244.0	1991.8	1976.8	10070.5	.020	8101.7	8253.9	0.0	0.0	0.0	.958	2.44
245.0	2001.5	1986.5	9724.3	.031	8108.3	8260.4	0.0	0.0	0.0	.957	2.37
246.0	2010.9	1995.9	9413.9	.064	8113.6	8265.4	0.0	0.0	0.0	.973	2.19
247.0	2019.9	2004.9	8954.6	0.000	8117.0	8268.3	0.0	0.0	0.0	.973	2.16
248.0	2030.1	2015.1	10116.2	-.013	8125.3	8276.8	0.0	0.0	0.0	.973	2.21
249.0	2040.3	2025.3	10214.7	.027	8133.7	8285.5	0.0	0.0	0.0	.973	2.13
250.0	2050.3	2035.3	10016.2	.003	8141.2	8293.2	0.0	0.0	0.0	.973	2.17
251.0	2060.1	2045.1	9775.6	-.007	8147.7	8299.6	0.0	0.0	0.0	.972	2.16
252.0	2070.0	2055.0	9962.7	.005	8154.9	8306.9	0.0	0.0	0.0	.972	2.11
253.0	2080.1	2065.1	10099.8	-.009	8162.6	8314.7	0.0	0.0	0.0	.972	2.11
254.0	2090.4	2075.4	10293.1	.000	8171.0	8323.4	0.0	0.0	0.0	.972	2.09
255.0	2100.0	2085.8	10383.6	-.004	8179.7	8332.5	0.0	0.0	0.0	.972	2.09
256.0	2111.3	2096.3	10451.5	-.031	8188.5	8341.6	0.0	0.0	0.0	.972	2.10
257.0	2121.5	2106.9	10630.9	.010	8199.1	8352.0	0.0	0.0	0.0	.972	2.06
258.0	2132.0	2117.6	10649.7	.002	8207.6	8362.1	0.0	0.0	0.0	.972	2.07
259.0	2143.1	2128.1	10548.4	.010	8216.6	8371.6	0.0	0.0	0.0	.972	2.05
260.0	2153.5	2139.5	10438.2	-.004	8225.2	8380.6	0.0	0.0	0.0	.972	2.05

T	DKB	DDP	IV	K	VAV	VAMS	0.	0.	ALPHA	DENS
							DT FOR K =			
261.0	2164.0	2149.0	10470.0	-.012	8233.8	8369.6	0.0	0.0	.972	2.06
262.0	2174.3	2159.3	10285.2	-.024	8241.6	8397.6	0.0	0.0	.971	2.03
263.0	2185.1	2170.1	10845.3	-.004	8251.5	8408.3	0.0	0.0	.971	2.03
264.0	2195.9	2180.9	10748.5	-.012	8260.9	8418.4	0.0	0.0	.971	2.03
265.0	2206.9	2191.9	11000.1	.018	8271.3	8429.6	0.0	0.0	.971	2.01
266.0	2217.6	2202.6	10724.6	.009	8280.5	8439.4	0.0	0.0	.971	2.00
267.0	2228.2	2213.2	10576.5	.002	8289.1	8448.4	0.0	0.0	.971	2.00
268.0	2238.7	2223.7	10542.8	-.020	8297.5	8457.2	0.0	0.0	.970	2.00
269.0	2249.7	2234.7	10976.6	-.014	8307.5	8468.0	0.0	0.0	.970	2.02
270.0	2260.9	2245.9	11172.6	-.004	8318.1	8479.6	0.0	0.0	.970	2.05
271.0	2272.0	2257.0	11088.1	.026	8328.3	8490.7	0.0	0.0	.970	2.02
272.0	2282.7	2267.7	10715.0	-.010	8337.1	8499.9	0.0	0.0	.969	2.01
273.0	2293.7	2278.7	10987.3	.012	8346.8	8510.3	0.0	0.0	.969	2.00
274.0	2304.4	2289.4	10752.5	.012	8355.6	8519.6	0.0	0.0	.969	2.00
275.0	2314.9	2299.9	10504.7	.004	8363.4	8527.7	0.0	0.0	.969	2.00
276.0	2325.3	2310.3	10329.3	.001	8370.5	8534.9	0.0	0.0	.969	2.00
277.0	2335.6	2320.6	10304.9	.005	8377.5	8541.9	0.0	0.0	.969	2.00
278.0	2345.8	2330.8	10204.7	.017	8384.1	8548.5	0.0	0.0	.969	2.00
279.0	2355.6	2340.6	9967.3	.013	8389.4	8553.6	0.0	0.0	.969	2.00
280.0	2365.2	2350.2	9607.8	.011	8393.7	8557.6	0.0	0.0	.969	2.00

I	UXB	DDP	IV	K	VAV	VRMS	0.	0.	0.	ALPHA	DENS
							OT FOR X =				
261.0	2374.6	2359.6	9472.5	-.005	8397.3	8560.7	0.0	0.0	0.0	.968	2.00
262.0	2344.1	2369.1	9760.3	-.016	8401.1	8564.1	0.0	0.0	0.0	.969	2.01
263.0	2393.9	2370.9	9769.4	-.001	8405.9	8568.6	0.0	0.0	0.0	.968	2.01
264.0	2403.7	2389.7	9732.3	.003	8410.8	8573.2	0.0	0.0	0.0	.968	2.01
265.0	2413.4	2398.4	9727.5	-.001	8415.4	8577.6	0.0	0.0	0.0	.968	2.01
266.0	2423.1	2408.1	9926.7	-.014	8420.0	8581.9	0.0	0.0	0.0	.968	2.03
267.0	2433.1	2417.1	10480.5	-.041	8425.3	8586.9	0.0	0.0	0.0	.966	2.09
268.0	2443.5	2426.5	10952.1	-.033	8432.4	8594.2	0.0	0.0	0.0	.965	2.14
269.0	2454.5	2435.5	10711.0	.014	8441.1	8603.5	0.0	0.0	0.0	.965	2.12
290.0	2465.2	2450.2	10826.9	-.004	8448.9	8611.6	0.0	0.0	0.0	.965	2.12
291.0	2476.0	2461.0	10448.6	.025	8457.1	8620.2	0.0	0.0	0.0	.964	2.07
292.0	2486.5	2472.5	9465.8	0.000	8463.9	8627.1	0.0	0.0	0.0	.964	2.07
293.0	2495.9	2480.9	9604.7	-.015	8467.4	8630.1	0.0	0.0	0.0	.964	2.10
294.0	2505.5	2490.5	9660.3	-.012	8471.2	8633.6	0.0	0.0	0.0	.964	2.14
295.0	2515.2	2500.2	9799.6	-.003	8475.3	8637.3	0.0	0.0	0.0	.964	2.12
296.0	2525.0	2510.0	9264.9	.036	8479.7	8641.5	0.0	0.0	0.0	.963	2.09
297.0	2534.3	2519.3	9373.1	-.011	8482.4	8643.7	0.0	0.0	0.0	.963	2.11
298.0	2543.6	2529.6	9815.2	-.037	8485.3	8646.2	0.0	0.0	0.0	.961	2.17
299.0	2553.4	2538.4	10023.9	-.014	8489.8	8650.4	0.0	0.0	0.0	.961	2.21
300.0	2563.5	2548.5		.005	8494.9	8655.3	0.0	0.0	0.0	.961	2.21

T	DKB	DDP	IV	K	VAV	VRMS	DT FOR X			ALPHA	DENS
301.0	2573.5	2598.5	9991.5	-.014	8459.9	8660.1	0.0	0.0	0.0	.961	2.20
302.0	2583.4	2560.4	9869.7	.016	8504.5	8664.5	0.0	0.0	0.0	.960	2.19
303.0	2593.2	2576.2	9702.7	.027	8509.0	8668.7	0.0	0.0	0.0	.960	2.02
304.0	2602.9	2587.9	9264.2	.024	8512.9	8672.4	0.0	0.0	0.0	.959	2.01
305.0	2612.2	2597.2	9006.0	.017	8515.5	8674.4	0.0	0.0	0.0	.959	2.06
306.0	2621.2	2606.2	8876.9	.007	8517.1	8675.5	0.0	0.0	0.0	.959	2.00
307.0	2630.1	2615.1	9142.0	-.015	8518.2	8676.2	0.0	0.0	0.0	.959	2.06
308.0	2639.1	2624.2	9045.0	.005	8520.3	8677.8	0.0	0.0	0.0	.959	2.00
309.0	2648.3	2633.3	8534.1	.029	8522.0	8679.0	0.0	0.0	0.0	.958	2.00
310.0	2656.8	2641.8	8912.8	-.028	8522.0	8676.5	0.0	0.0	0.0	.957	2.03
311.0	2665.7	2650.7	9208.2	-.017	8523.3	8679.3	0.0	0.0	0.0	.957	2.03
312.0	2674.9	2659.9	9330.5	-.004	8525.5	8691.0	0.0	0.0	0.0	.957	2.02
313.0	2684.3	2669.3	9507.4	-.011	8528.0	8683.2	0.0	0.0	0.0	.957	2.03
314.0	2693.8	2678.8	9736.1	-.013	8531.1	8685.9	0.0	0.0	0.0	.956	2.03
315.0	2703.5	2688.5	9906.3	.027	8535.0	8689.4	0.0	0.0	0.0	.956	2.01
316.0	2712.8	2697.8	9608.5	-.013	8537.4	8691.5	0.0	0.0	0.0	.956	2.00
317.0	2722.4	2707.4	9952.0	-.019	8540.8	8694.5	0.0	0.0	0.0	.955	2.01
318.0	2732.4	2717.4	9988.2	-.002	8545.2	8698.8	0.0	0.0	0.0	.955	2.01
319.0	2742.4	2727.4	9532.7	.021	8549.8	8703.1	0.0	0.0	0.0	.955	2.02
320.0	2751.9	2736.9		-.035	8552.9	8705.8	0.0	0.0	0.0		

T	DKB	DDP	IV	K	VAV	VRMS	DT FOR X = 0.	0.	0.	ALPHA	DENS
321.0	2761.9	2746.9	9952.4	-.034	8557.2	8710.0	0.0	0.0	0.0	.954	2.08
322.0	2772.2	2757.2	10309.9	.004	8562.6	8715.4	0.0	0.0	0.0	.953	2.15
323.0	2782.5	2767.5	10296.8	.019	8568.0	8720.7	0.0	0.0	0.0	.952	2.13
324.0	2792.4	2777.4	9970.4	.008	8572.3	8724.9	0.0	0.0	0.0	.952	2.12
325.0	2802.5	2787.5	10054.1	-.004	8576.9	8729.3	0.0	0.0	0.0	.952	2.07
326.0	2812.8	2797.8	10321.9	.005	8582.2	8734.6	0.0	0.0	0.0	.952	2.03
327.0	2823.1	2808.1	10253.1	.011	8587.3	8739.6	0.0	0.0	0.0	.952	2.02
328.0	2833.2	2818.2	10111.2	.007	8592.0	8744.2	0.0	0.0	0.0	.952	2.01
329.0	2843.2	2828.2	10003.8	.002	8596.3	8748.3	0.0	0.0	0.0	.952	2.00
330.0	2853.1	2838.1	9931.3	.011	8600.3	8752.1	0.0	0.0	0.0	.952	2.01
331.0	2862.8	2847.3	9657.1	.001	8603.5	8755.0	0.0	0.0	0.0	.952	2.02
332.0	2872.4	2857.4	9537.9	-.025	8606.6	8757.8	0.0	0.0	0.0	.952	2.02
333.0	2882.5	2867.5	10099.4	-.002	8611.1	8762.1	0.0	0.0	0.0	.951	2.02
334.0	2892.6	2877.6	10084.4	-.010	8615.5	8766.3	0.0	0.0	0.0	.951	2.04
335.0	2902.7	2887.7	10105.5	-.062	8620.0	8770.7	0.0	0.0	0.0	.951	2.07
336.0	2913.2	2898.2	10512.6	-.059	8625.6	8776.3	0.0	0.0	0.0	.947	2.25
337.0	2924.3	2909.3	11113.2	.004	8633.0	8784.2	0.0	0.0	0.0	.944	2.40
338.0	2935.4	2920.4	11086.5	.023	8640.3	8791.9	0.0	0.0	0.0	.944	2.39
339.0	2946.1	2931.1	10742.5	-.005	8646.5	8798.3	0.0	0.0	0.0	.944	2.35
340.0	2956.9	2941.9	10788.4	-.014	8652.8	8804.8	0.0	0.0	0.0	.944	2.37

T	DKB	DDP	LV	K	VAV	VRMS	DT FOR X = 0.	0.	ALPHA	DENS
341.0	2967.6	2552.8	10892.7	.008	8659.3	8811.7	0.0	0.0	.943	2.41
342.0	2978.6	2963.6	10766.5	.003	8665.5	8818.0	0.0	0.0	.943	2.39
343.0	2989.3	2974.3	10726.2	-.002	8671.5	8824.2	0.0	0.0	.943	2.40
344.0	3000.0	2985.0	10726.7	-.007	8677.5	8830.3	0.0	0.0	.943	2.39
345.0	3011.0	2996.0	10904.4	-.017	8683.9	8837.0	0.0	0.0	.943	2.42
346.0	3022.1	3007.1	11145.5	.011	8691.0	8844.5	0.0	0.0	.943	2.43
347.0	3033.0	3018.0	10876.2	-.008	8697.3	8851.1	0.0	0.0	.943	2.43
348.0	3044.0	3029.0	11027.4	.005	8704.0	8858.1	0.0	0.0	.943	2.43
349.0	3055.0	3040.0	10549.3	-.004	8710.5	8864.8	0.0	0.0	.943	2.44
350.0	3065.9	3050.9	10968.7	-.011	8716.9	8871.5	0.0	0.0	.943	2.45
351.0	3077.1	3062.1	11179.3	.008	8723.9	8878.9	0.0	0.0	.943	2.44
352.0	3088.1	3073.1	11041.0	.018	8730.5	8885.8	0.0	0.0	.942	2.41
353.0	3096.9	3083.9	10792.9	.002	8736.4	8891.8	0.0	0.0	.942	2.41
354.0	3109.7	3094.7	10745.1	-.000	8742.0	8897.6	0.0	0.0	.942	2.40
355.0	3121.5	3105.5	10782.3	-.050	8747.8	8903.4	0.0	0.0	.940	2.42
356.0	3132.3	3117.3	11132.1	0.000	8756.4	8913.0	0.0	0.0	.940	2.43
357.0	3144.7	3129.7	12416.6	.004	8766.7	8924.8	0.0	0.0	.940	2.43
358.0	3157.0	3142.0	12248.6	-.014	8776.4	8935.8	0.0	0.0	.940	2.41
359.0	3169.6	3154.6	12644.0	-.055	8787.2	8948.2	0.0	0.0	.937	2.48
360.0	3183.4	3166.4	13761.3	.093	8801.0	8965.2	0.0	0.0		

I	DKB	DDP	IV	K	VAV	VRMS	Q.	Q.	Q.	ALPHA	DENS
							DT FOR X =				
361.0	3197.0	3182.0	13668.1	.017	6814.5	6981.6	0.0	0.0	0.0	.937	2.48
362.0	3210.3	3195.3	13271.0	-.022	6826.8	6996.3	0.0	0.0	0.0	.936	2.48
363.0	3224.1	3209.1	13700.7	-.011	6840.5	9012.9	0.0	0.0	0.0	.936	2.49
364.0	3238.1	3223.1	14040.6	.042	6854.7	9030.6	0.0	0.0	0.0	.935	2.45
365.0	3251.2	3236.2	13093.0	-.023	6866.4	9044.2	0.0	0.0	0.0	.934	2.46
366.0	3264.9	3249.9	13637.3	-.008	6879.4	9059.9	0.0	0.0	0.0	.934	2.48
367.0	3278.6	3263.6	13741.4	-.021	6892.6	9076.0	0.0	0.0	0.0	.934	2.47
368.0	3292.9	3277.9	14352.4	-.037	6907.9	9094.5	0.0	0.0	0.0	.934	2.49
369.0	3307.4	3292.4	14499.9	-.032	6922.6	9113.4	0.0	0.0	0.0	.934	2.48
370.0	3322.0	3307.0	14557.7	-.031	6937.9	9132.5	0.0	0.0	0.0	.934	2.48
371.0	3336.6	3321.6	14587.7	.014	6953.1	9151.6	0.0	0.0	0.0	.933	2.49
372.0	3396.7	3395.7	14121.2	.006	6967.0	9168.6	0.0	0.0	0.0	.933	2.49
373.0	3364.7	3349.7	13956.1	.004	6980.4	9184.8	0.0	0.0	0.0	.933	2.47
374.0	3378.6	3363.6	13940.0	-.003	6993.6	9200.7	0.0	0.0	0.0	.933	2.48
375.0	3392.6	3377.6	13965.5	-.006	7006.9	9216.7	0.0	0.0	0.0	.933	2.49
376.0	3406.7	3391.7	14100.5	-.006	7020.4	9233.1	0.0	0.0	0.0	.933	2.49
377.0	3420.9	3405.9	14260.5	-.006	7034.3	9250.1	0.0	0.0	0.0	.933	2.48
378.0	3434.9	3419.9	13960.2	.002	7047.4	9265.7	0.0	0.0	0.0	.933	2.48
379.0	3449.0	3433.8	13869.2	.003	7060.1	9280.9	0.0	0.0	0.0	.933	2.48
380.0	3462.3	3447.3	13547.3	.014	7071.9	9294.7	0.0	0.0	0.0	.933	2.47

T	DKB	DDP	IV	K	VAV	VRMS	D1 FOR X = 0.	0.	0.	ALPHA	DENS
381.0	3475.9	3460.9	13564.7	.029	9083.7	9308.4	0.0	0.0	0.0	.933	2.48
382.0	3489.1	3474.1	13245.9	.018	9094.6	9320.9	0.0	0.0	0.0	.932	2.39
383.0	3502.3	3487.3	13147.1	.011	9105.2	9332.9	0.0	0.0	0.0	.932	2.33
384.0	3515.1	3500.1	12847.6	-.012	9114.9	9343.8	0.0	0.0	0.0	.932	2.33
385.0	3528.2	3513.2	13055.3	-.004	9125.1	9355.4	0.0	0.0	0.0	.932	2.35
386.0	3541.1	3526.1	12897.5	-.001	9134.9	9366.3	0.0	0.0	0.0	.932	2.40
387.0	3553.9	3538.9	12871.8	.007	9144.6	9377.0	0.0	0.0	0.0	.932	2.41
388.0	3566.6	3551.6	12624.5	.013	9153.5	9386.8	0.0	0.0	0.0	.931	2.42
389.0	3578.9	3563.9	12306.3	-.012	9161.6	9395.5	0.0	0.0	0.0	.931	2.42
390.0	3591.5	3576.5	12620.9	.002	9170.5	9405.2	0.0	0.0	0.0	.931	2.42
391.0	3604.2	3589.2	12692.8	.022	9179.5	9415.1	0.0	0.0	0.0	.931	2.40
392.0	3616.4	3601.4	12187.3	.004	9187.2	9423.2	0.0	0.0	0.0	.931	2.39
393.0	3628.6	3613.6	12231.7	-.022	9194.9	9431.4	0.0	0.0	0.0	.931	2.36
394.0	3641.3	3626.3	12738.1	.010	9203.9	9441.2	0.0	0.0	0.0	.930	2.37
395.0	3653.9	3638.9	12523.2	-.006	9212.3	9450.3	0.0	0.0	0.0	.930	2.36
396.0	3666.7	3651.7	12824.8	-.007	9221.5	9460.3	0.0	0.0	0.0	.930	2.33
397.0	3679.9	3664.9	13240.1	.007	9231.6	9471.8	0.0	0.0	0.0	.930	2.29
398.0	3693.3	3678.3	13322.0	.025	9241.9	9483.4	0.0	0.0	0.0	.930	2.25
399.0	3706.3	3691.3	13024.7	.037	9251.3	9493.9	0.0	0.0	0.0	.930	2.19
400.0	3718.7	3703.9	12616.4	-.027	9259.7	9503.0	0.0	0.0	0.0	.928	2.10

T	OKB	OOP	IV	K	VAV	VRMS	DT FOR X = 0.	0.	0.	ALPHA	DENS
401.0	3732.3	3717.3	13367.5	.008	9270.0	9514.6	0.0	0.0	0.0	.928	2.09
402.0	3745.4	3730.4	13127.3	-.009	9279.6	9525.3	0.0	0.0	0.0	.927	2.14
403.0	3758.5	3743.5	13077.5	-.006	9269.0	9535.7	0.0	0.0	0.0	.927	2.11
404.0	3771.9	3756.9	13423.6	.003	9299.2	9547.3	0.0	0.0	0.0	.927	2.06
405.0	3785.5	3770.5	13574.6	.012	9309.8	9559.3	0.0	0.0	0.0	.927	2.03
406.0	3799.0	3784.0	13937.5	-.030	9320.2	9571.2	0.0	0.0	0.0	.926	2.06
407.0	3813.2	3796.2	14212.4	-.016	9332.2	9585.3	0.0	0.0	0.0	.926	2.07
408.0	3827.8	3812.8	14544.8	.013	9345.0	9600.6	0.0	0.0	0.0	.926	2.05
409.0	3842.1	3827.1	14331.0	-.013	9357.2	9615.0	0.0	0.0	0.0	.926	2.05
410.0	3856.8	3841.8	14697.1	-.000	9370.2	9630.7	0.0	0.0	0.0	.926	2.08
411.0	3871.3	3856.3	14500.6	.012	9382.7	9645.5	0.0	0.0	0.0	.926	2.10
412.0	3885.5	3870.5	14190.1	.008	9394.4	9659.1	0.0	0.0	0.0	.926	2.07
413.0	3899.5	3884.5	14013.9	.040	9405.6	9672.0	0.0	0.0	0.0	.924	2.09
414.0	3912.3	3897.3	12801.7	.016	9413.8	9680.8	0.0	0.0	0.0	.924	2.08
415.0	3924.0	3909.0	12459.6	-.032	9421.1	9688.5	0.0	0.0	0.0	.923	2.09
416.0	3936.0	3923.0	13202.4	-.010	9430.2	9698.5	0.0	0.0	0.0	.923	2.10
417.0	3951.4	3936.4	13452.7	-.007	9439.8	9709.2	0.0	0.0	0.0	.923	2.04
418.0	3965.1	3950.1	13733.6	.010	9450.1	9720.8	0.0	0.0	0.0	.923	2.07
419.0	3978.7	3963.7	13552.6	.001	9459.9	9731.8	0.0	0.0	0.0	.923	2.07
420.0	3992.2	3977.2	13510.9	-.030	9469.5	9742.5	0.0	0.0	0.0	.923	2.07

I	DKB	DDF	IV	K	VAV	VRMS	0.	0.	DT FUR X =	0.	ALPHA	DENS
421.0	4006.3	3991.3	14117.3	.003	9480.6	9755.2	0.0	0.0	0.0	0.0	.922	2.11
422.0	4020.2	4005.2	13912.8	.024	9491.1	9767.2	0.0	0.0	0.0	0.0	.922	2.13
423.0	4033.3	4018.3	13061.4	-.010	9499.6	9776.3	0.0	0.0	0.0	0.0	.921	2.14
424.0	4046.7	4031.7	13337.7	-.005	9508.6	9786.2	0.0	0.0	0.0	0.0	.921	2.14
425.0	4060.1	4045.1	13462.4	-.001	9517.9	9796.5	0.0	0.0	0.0	0.0	.921	2.15
426.0	4073.5	4058.5	13421.1	.014	9527.1	9806.6	0.0	0.0	0.0	0.0	.921	2.19
427.0	4086.4	4071.4	12015.8	-.007	9534.8	9814.7	0.0	0.0	0.0	0.0	.921	2.21
428.0	4099.2	4084.2	12848.0	-.005	9542.5	9822.9	0.0	0.0	0.0	0.0	.921	2.24
429.0	4112.1	4097.1	12652.8	-.023	9550.3	9831.0	0.0	0.0	0.0	0.0	.920	2.30
430.0	4125.1	4110.1	14071.6	-.044	9558.4	9839.8	0.0	0.0	0.0	0.0	.919	2.39
431.0	4138.9	4123.9	13799.8	-.009	9566.2	9850.7	0.0	0.0	0.0	0.0	.919	2.47
432.0	4152.4	4137.4	13552.7	.019	9577.4	9860.9	0.0	0.0	0.0	0.0	.918	2.46
433.0	4165.5	4150.5	13105.7	.013	9585.6	9869.6	0.0	0.0	0.0	0.0	.918	2.48
434.0	4178.2	4163.2	12670.3	-.009	9592.7	9877.3	0.0	0.0	0.0	0.0	.918	2.50
435.0	4191.0	4176.0	12793.5	-.015	9600.0	9884.7	0.0	0.0	0.0	0.0	.918	2.50
436.0	4204.4	4189.2	13143.5	-.016	9608.2	9893.5	0.0	0.0	0.0	0.0	.918	2.51
437.0	4217.7	4202.7	13547.9	.003	9617.3	9903.4	0.0	0.0	0.0	0.0	.918	2.50
438.0	4231.2	4216.2	13490.0	-.001	9626.1	9913.1	0.0	0.0	0.0	0.0	.918	2.51
439.0	4244.7	4229.7	13473.1	-.011	9634.9	9922.6	0.0	0.0	0.0	0.0	.917	2.52
440.0	4258.4	4243.4	13695.6	-.005	9644.1	9932.8	0.0	0.0	0.0	0.0	.917	2.52

T	DKB	DDP	IV	K	VAV	VRMS	0.	0.	0.	ALPHA	DENS
						DT FOR X =					
441.0	4272.2	4257.2	13756.2	.034	9653.4	9943.2	0.0	0.0	0.0	.917	2.53
442.0	4285.2	4270.2	13017.3	.017	9661.0	9951.2	0.0	0.0	0.0	.916	2.51
443.0	4297.7	4282.7	12541.7	-.002	9667.5	9957.8	0.0	0.0	0.0	.916	2.51
444.0	4310.2	4295.3	12566.7	-.014	9674.1	9964.4	0.0	0.0	0.0	.916	2.51
445.0	4323.2	4308.2	12955.3	-.014	9681.4	9972.2	0.0	0.0	0.0	.916	2.53
446.0	4336.3	4321.3	13102.2	-.016	9689.1	9980.3	0.0	0.0	0.0	.916	2.52
447.0	4349.9	4334.9	13571.1	-.014	9697.6	9989.8	0.0	0.0	0.0	.915	2.53
448.0	4363.0	4348.0	13926.4	-.011	9707.2	10000.3	0.0	0.0	0.0	.915	2.53
449.0	4378.1	4363.1	14246.7	-.005	9717.3	10011.7	0.0	0.0	0.0	.915	2.54
450.0	4392.4	4377.4	14299.2	-.010	9727.5	10023.3	0.0	0.0	0.0	.915	2.54
451.0	4407.0	4392.0	14412.9	.016	9738.4	10035.8	0.0	0.0	0.0	.915	2.55
452.0	4421.1	4406.1	14123.0	.025	9748.1	10046.7	0.0	0.0	0.0	.914	2.52
453.0	4434.7	4419.7	13606.6	.003	9756.6	10055.9	0.0	0.0	0.0	.914	2.53
454.0	4448.3	4433.3	13531.6	-.017	9764.9	10064.9	0.0	0.0	0.0	.914	2.54
455.0	4462.2	4447.2	13938.2	.008	9774.1	10075.0	0.0	0.0	0.0	.914	2.54
456.0	4475.9	4460.9	13698.1	-.002	9782.7	10084.4	0.0	0.0	0.0	.914	2.52
457.0	4489.0	4474.0	13962.7	.007	9791.6	10094.2	0.0	0.0	0.0	.914	2.53
458.0	4503.4	4488.4	13615.1	-.001	9799.9	10103.2	0.0	0.0	0.0	.914	2.53
459.0	4517.1	4502.1	13706.9	-.005	9808.5	10112.5	0.0	0.0	0.0	.914	2.52
460.0	4531.1	4516.1	13995.1	.000	9817.6	10122.5	0.0	0.0	0.0	.914	2.52

T	DKB	DDP	IV	K	VAV	VRMS	DT FOR X = 0.	0.	0.	ALPHA	DENS
461.0	4545.1	4530.1	14039.1	.000	9826.7	10132.7	0.0	0.0	0.0	.914	2.51
462.0	4559.2	4544.2	14078.5	.007	9835.9	10142.9	0.0	0.0	0.0	.914	2.50
463.0	4573.3	4558.3	14067.6	-.008	9845.1	10153.0	0.0	0.0	0.0	.914	2.47
464.0	4587.4	4572.4	14108.0	-.004	9854.2	10163.2	0.0	0.0	0.0	.914	2.51
465.0	4601.6	4586.6	14230.4	.007	9863.7	10173.7	0.0	0.0	0.0	.914	2.51
466.0	4615.9	4600.9	14250.9	-.003	9873.1	10184.1	0.0	0.0	0.0	.914	2.47
467.0	4630.3	4615.3	14418.9	-.002	9882.8	10195.1	0.0	0.0	0.0	.914	2.45
468.0	4644.8	4629.8	14534.7	-.011	9892.7	10206.3	0.0	0.0	0.0	.914	2.44
469.0	4659.4	4644.4	14629.9	-.002	9902.8	10217.8	0.0	0.0	0.0	.914	2.48
470.0	4674.0	4659.0	14525.5	.003	9912.7	10228.9	0.0	0.0	0.0	.914	2.51
471.0	4688.3	4673.3	14387.5	-.002	9922.2	10239.5	0.0	0.0	0.0	.914	2.52
472.0	4702.9	4687.9	14524.3	-.006	9931.9	10250.5	0.0	0.0	0.0	.914	2.51
473.0	4717.6	4702.6	14752.2	.032	9942.1	10262.1	0.0	0.0	0.0	.914	2.50
474.0	4731.5	4716.5	13875.5	-.040	9950.4	10271.0	0.0	0.0	0.0	.913	2.49
475.0	4746.5	4731.5	15046.1	-.017	9961.1	10283.4	0.0	0.0	0.0	.911	2.49
476.0	4762.2	4747.2	15609.1	-.006	9973.0	10297.5	0.0	0.0	0.0	.911	2.48
477.0	4777.9	4762.9	15720.2	.021	9985.1	10311.9	0.0	0.0	0.0	.911	2.50
478.0	4793.0	4778.0	15112.3	.004	9995.8	10324.2	0.0	0.0	0.0	.910	2.49
479.0	4807.9	4792.9	14920.9	.033	10006.1	10336.0	0.0	0.0	0.0	.910	2.50
480.0	4822.0	4807.0	14066.6	-.005	10014.5	10345.1	0.0	0.0	0.0	.909	2.48

I	DKB	DDP	IV	K	VAV	VRMS	DT FOR X =	0.	0.	ALPHA	DENS
481.0	4830.1	4621.1	14073.1	-.035	10023.0	10354.3	0.0	0.0	0.0	.909	2.50
482.0	4851.3	4836.3	15200.6	.005	10033.7	10366.7	0.0	0.0	0.0	.908	2.49
483.0	4866.4	4851.4	19139.0	.013	10044.3	10378.8	0.0	0.0	0.0	.909	2.47
484.0	4880.9	4865.9	14531.6	-.003	10053.5	10389.1	0.0	0.0	0.0	.908	2.50
485.0	4895.5	4880.5	14613.0	.026	10062.9	10399.6	0.0	0.0	0.0	.907	2.45
486.0	4909.7	4894.7	14161.5	.001	10071.4	10408.7	0.0	0.0	0.0	.907	2.48
487.0	4923.6	4908.6	13947.6	-.023	10079.3	10417.2	0.0	0.0	0.0	.907	2.50
488.0	4936.1	4923.1	14453.6	.005	10088.3	10427.1	0.0	0.0	0.0	.907	2.49
489.0	4952.5	4937.5	14414.3	.001	10097.2	10436.8	0.0	0.0	0.0	.907	2.52
490.0	4966.7	4951.7	14191.5	-.006	10105.5	10445.8	0.0	0.0	0.0	.907	2.51
491.0	4991.1	4966.1	14429.7	.005	10114.3	10455.5	0.0	0.0	0.0	.907	2.50
492.0	4995.3	4980.3	14197.5	-.003	10122.6	10464.4	0.0	0.0	0.0	.907	2.54
493.0	5009.4	4994.4	14089.8	-.010	10130.7	10473.1	0.0	0.0	0.0	.907	2.54
494.0	5023.7	5008.7	14328.3	-.019	10139.2	10482.3	0.0	0.0	0.0	.906	2.56
495.0	5038.6	5023.6	14806.9	.006	10148.6	10492.8	0.0	0.0	0.0	.906	2.56
496.0	5053.1	5038.1	14584.9	.034	10157.5	10502.7	0.0	0.0	0.0	.905	2.52
497.0	5067.0	5052.0	13830.6	.008	10166.9	10510.4	0.0	0.0	0.0	.905	2.52
498.0	5080.6	5065.6	13619.3	.004	10171.9	10517.6	0.0	0.0	0.0	.905	2.52
499.0	5094.1	5079.1	13547.5	.006	10178.6	10524.6	0.0	0.0	0.0	.905	2.49
500.0	5107.7	5092.7	13524.3	.006	10185.3	10531.4	0.0	0.0	0.0	.905	2.49

T	DKB	DOP	IV	K	VAV	VRMS	DT FOR X = 0.	0.	0.	ALPHA	DENS
501.0	5121.0	5106.0	13391.7	.000	10191.7	10537.9	0.0	0.0	0.0	.905	2.48
502.0	5134.7	5119.7	13632.4	.007	10198.6	10545.0	0.0	0.0	0.0	.905	2.43
503.0	5148.3	5133.3	13664.6	.048	10205.5	10552.1	0.0	0.0	0.0	.905	2.39
504.0	5161.7	5146.7	13391.2	.009	10211.8	10558.5	0.0	0.0	0.0	.903	2.21
505.0	5175.0	5160.0	13251.7	-.031	10217.8	10564.5	0.0	0.0	0.0	.903	2.20
506.0	5189.1	5174.1	14084.2	.007	10225.4	10572.6	0.0	0.0	0.0	.902	2.20
507.0	5203.0	5188.0	13929.7	.004	10232.7	10580.3	0.0	0.0	0.0	.902	2.19
508.0	5217.1	5202.1	14062.4	-.031	10240.3	10588.2	0.0	0.0	0.0	.902	2.15
509.0	5232.2	5217.2	15098.1	-.014	10249.8	10599.0	0.0	0.0	0.0	.901	2.13
510.0	5247.7	5232.7	15493.2	.034	10260.1	10610.8	0.0	0.0	0.0	.901	2.14
511.0	5262.1	5247.1	14431.7	.028	10268.3	10619.6	0.0	0.0	0.0	.900	2.15
512.0	5276.2	5261.2	14158.1	-.016	10275.9	10627.7	0.0	0.0	0.0	.899	2.07
513.0	5290.8	5275.8	14600.3	-.005	10284.3	10635.9	0.0	0.0	0.0	.899	2.07
514.0	5305.5	5290.5	14670.3	-.016	10292.8	10646.2	0.0	0.0	0.0	.899	2.08
515.0	5320.6	5305.6	15120.0	-.039	10302.2	10656.7	0.0	0.0	0.0	.899	2.09
516.0	5336.7	5321.7	16103.1	-.010	10313.5	10669.9	0.0	0.0	0.0	.897	2.12
517.0	5353.0	5338.0	16285.2	.003	10325.0	10683.6	0.0	0.0	0.0	.897	2.14
518.0	5369.3	5354.3	16272.9	.001	10336.5	10697.2	0.0	0.0	0.0	.897	2.12
519.0	5385.5	5370.5	16189.0	.014	10347.8	10710.5	0.0	0.0	0.0	.897	2.13
520.0	5401.2	5386.2	15697.2	-.010	10358.0	10722.4	0.0	0.0	0.0	.897	2.14

T	OKD	DDP	IV	K	VAV	VRMS	DT FOR X = 0.	0.	0.	ALPHA	DENS
			15706.9							.897	2.18
521.0	5416.9	5401.9		-.008	10368.3	10734.1	0.0	0.0	0.0		
			15753.0							.897	2.21
522.0	5432.6	5417.6		.006	10378.6	10746.0	0.0	0.0	0.0		
			15780.8							.897	2.18
523.0	5448.4	5433.4		-.006	10389.0	10757.9	0.0	0.0	0.0		
			15954.5							.897	2.18
524.0	5464.4	5449.4		.002	10399.6	10770.2	0.0	0.0	0.0		
			16036.3							.897	2.16
525.0	5480.4	5465.4		.027	10410.3	10782.7	0.0	0.0	0.0		
			15574.8							.896	2.11
526.0	5496.0	5481.0		.047	10420.2	10793.8	0.0	0.0	0.0		
			14605.3							.894	2.05
527.0	5510.6	5495.6		.030	10428.1	10802.3	0.0	0.0	0.0		
			14031.8							.893	2.00
528.0	5524.6	5509.6		-.032	10434.9	10809.3	0.0	0.0	0.0		
			14909.6							.893	2.01
529.0	5539.5	5524.5		-.010	10443.4	10818.6	0.0	0.0	0.0		
			15280.0							.892	2.00
530.0	5554.8	5539.8		-.005	10452.5	10828.7	0.0	0.0	0.0		
			15423.6							.892	2.00
531.0	5571.3	5555.3		-.003	10461.9	10839.2	0.0	0.0	0.0		
			15516.4							.892	2.00
532.0	5585.8	5570.8		-.002	10471.4	10849.9	0.0	0.0	0.0		
			15584.5							.892	2.00
533.0	5601.4	5586.4		-.007	10481.0	10860.7	0.0	0.0	0.0		
			15672.8							.892	2.02
534.0	5617.0	5602.0		-.002	10490.7	10871.7	0.0	0.0	0.0		
			15589.0							.892	2.04
535.0	5632.6	5617.6		-.007	10500.2	10882.4	0.0	0.0	0.0		
			15726.4							.892	2.05
536.0	5648.3	5633.3		-.008	10510.0	10893.5	0.0	0.0	0.0		
			15592.6							.892	2.10
537.0	5663.9	5648.9		0.000	10519.4	10904.1	0.0	0.0	0.0		
			14390.1							.892	2.19
538.0	5678.3	5663.3		-.016	10526.6	10911.6	0.0	0.0	0.0		
			13910.9							.892	2.34
539.0	5692.2	5677.2		-.027	10532.9	10917.9	0.0	0.0	0.0		
			14064.0							.891	2.44
540.0	5706.3	5691.3		-.019	10539.4	10924.6	0.0	0.0	0.0		

T	DXB	DDP	IV	K	VAV	VRMS			
541.0	5120.7	5705.7	14374.1	.000	10546.5	10932.0	0.0	0.0	0.0
542.0	5234.8	5719.8	14150.1	.001	10553.2	10938.8	0.0	0.0	0.0
543.0	5248.1	5733.1	13309.1	-.045	10558.3	10943.6	0.0	0.0	0.0
544.0	5262.5	5747.5	14414.9	-.009	10565.3	10951.0	0.0	0.0	0.0
545.0	5277.2	5762.2	14676.7	.007	10572.9	10959.0	0.0	0.0	0.0
546.0	5291.5	5776.5	14316.1	.050	10579.7	10966.1	0.0	0.0	0.0
547.0	5304.7	5789.7	13584.4	-.010	10586.5	10973.5	0.0	0.0	0.0
548.0	5316.3	5803.3	13577.0	-.036	10589.9	10975.8	0.0	0.0	0.0
549.0	5327.3	5817.3	14084.7	.000	10596.3	10982.3	0.0	0.0	0.0
550.0	5336.5	5831.5	14185.7	.008	10602.8	10989.9	0.0	0.0	0.0
551.0	5344.5	5845.6	14078.4	.012	10609.1	10995.3	0.0	0.0	0.0
552.0	5350.6	5859.6	14005.5	-.008	10615.3	11001.5	0.0	0.0	0.0
553.0	5374.6	5874.1	14485.6	-.030	10622.3	11008.8	0.0	0.0	0.0
554.0	5389.1	5887.4	15342.3	-.034	10630.8	11016.2	0.0	0.0	0.0
555.0	5404.4	5895.6	16333.3	-.005	10641.0	11030.1	0.0	0.0	0.0
556.0	5920.8	5905.8	16921.2	-.011	10652.3	11043.5	0.0	0.0	0.0
557.0	5937.7	5922.7	17128.6	-.030	10664.0	11057.4	0.0	0.0	0.0
558.0	5954.9	5934.8	17489.8	-.020	10676.2	11072.3	0.0	0.0	0.0
559.0	5972.3	5997.3	17494.6	-.009	10688.4	11087.1	0.0	0.0	0.0
560.0	5989.8	5974.8	17519.2	-.002	10700.6	11101.9	0.0	0.0	0.0
561.0	6007.3	5992.3							

DEGS	ALPHA				
2.48	.891	0.0	0.0	0.0	0.0
2.52	.891	0.0	0.0	0.0	0.0
2.52	.890	0.0	0.0	0.0	0.0
2.55	.868	0.0	0.0	0.0	0.0
2.55	.888	0.0	0.0	0.0	0.0
2.57	.838	0.0	0.0	0.0	0.0
2.53	.886	0.0	0.0	0.0	0.0
2.50	.886	0.0	0.0	0.0	0.0
2.44	.886	0.0	0.0	0.0	0.0
2.42	.886	0.0	0.0	0.0	0.0
2.40	.886	0.0	0.0	0.0	0.0
2.36	.886	0.0	0.0	0.0	0.0
2.32	.886	0.0	0.0	0.0	0.0
2.33	.885	0.0	0.0	0.0	0.0
2.34	.884	0.0	0.0	0.0	0.0
2.28	.884	0.0	0.0	0.0	0.0
2.30	.884	0.0	0.0	0.0	0.0
2.39	.883	0.0	0.0	0.0	0.0
2.49	.883	0.0	0.0	0.0	0.0
2.54	.883	0.0	0.0	0.0	0.0

T	DKB	DDP	IV	K	VAV	VRMS	C.	C.	C.	ALPHA	DENS
					DT FOR X =		0.	0.	0.		
561.0	6024.7	6009.7	17409.3	-.001	10712.6	11116.3	0.0	0.0	0.0	.683	2.56
562.0	6042.2	6027.2	17455.0	.046	10724.6	11130.8	0.0	0.0	0.0	.681	2.54
563.0	6058.2	6043.2	16011.8	.028	10733.9	11141.4	0.0	0.0	0.0	.680	2.48
564.0	6073.8	6058.8	15567.9	-.040	10742.5	11150.8	0.0	0.0	0.0	.679	2.46
565.0	6090.6	6075.6	16026.2	-.027	10753.3	11163.4	0.0	0.0	0.0	.678	2.54
566.0	6108.0	6093.0	17375.8	-.013	10765.0	11177.4	0.0	0.0	0.0	.678	2.56
567.0	6125.5	6110.5	17557.5	.039	10777.0	11191.8	0.0	0.0	0.0	.677	2.52
568.0	6142.0	6127.0	16512.6	0.000	10787.1	11203.4	0.0	0.0	0.0	.677	2.53
569.0	6158.5	6143.5	16468.8	-.014	10797.0	11214.9	0.0	0.0	0.0	.676	2.55
570.0	6175.3	6160.3	16824.3	-.008	10807.6	11227.2	0.0	0.0	0.0	.676	2.59
571.0	6192.2	6177.2	16855.9	-.001	10818.2	11239.5	0.0	0.0	0.0	.676	2.58
572.0	6209.2	6194.2	16963.0	-.006	10829.0	11252.0	0.0	0.0	0.0	.676	2.60
573.0	6226.2	6211.2	17048.2	-.004	10839.8	11264.7	0.0	0.0	0.0	.676	2.60
574.0	6243.4	6228.4	17147.2	.002	10850.0	11277.7	0.0	0.0	0.0	.676	2.60
575.0	6260.4	6245.4	17093.1	.001	10861.7	11290.4	0.0	0.0	0.0	.676	2.59
576.0	6277.5	6262.5	17096.7	-.006	10872.5	11303.0	0.0	0.0	0.0	.675	2.61
577.0	6294.7	6279.7	17198.1	.009	10883.4	11315.9	0.0	0.0	0.0	.676	2.58
578.0	6311.9	6296.9	17067.6	.000	10894.1	11328.4	0.0	0.0	0.0	.676	2.57
579.0	6329.9	6313.9	17099.5	.007	10904.9	11340.9	0.0	0.0	0.0	.676	2.52
580.0	6346.2	6331.2	17260.6	.013	10915.8	11353.7	0.0	0.0	0.0	.676	2.52

T	DKB	DDP	IV	K	VAV	VRMS	DT FOR X = 0.	0.	0.	ALPHA	DENS
581.0	6363.3	6348.3	17161.5	-.006	10926.6	11366.3	0.0	0.0	0.0	.876	2.46
582.0	6380.6	6365.6	17288.2	.006	10937.5	11379.1	0.0	0.0	0.0	.876	2.48
583.0	6397.9	6382.9	17242.6	-.008	10948.3	11391.7	0.0	0.0	0.0	.876	2.46
584.0	6415.1	6400.1	17216.4	-.004	10959.0	11404.3	0.0	0.0	0.0	.876	2.50
585.0	6432.3	6417.3	17196.1	.009	10969.7	11416.7	0.0	0.0	0.0	.876	2.53
586.0	6449.5	6434.5	17243.2	-.006	10980.4	11429.1	0.0	0.0	0.0	.876	2.48
587.0	6466.8	6451.8	17236.6	-.003	10991.1	11441.5	0.0	0.0	0.0	.876	2.51
588.0	6483.9	6468.9	17149.9	.022	11001.5	11453.7	0.0	0.0	0.0	.876	2.53
589.0	6500.3	6485.3	16432.1	.019	11010.8	11464.0	0.0	0.0	0.0	.875	2.53
590.0	6516.2	6501.2	15830.6	-.028	11018.9	11472.8	0.0	0.0	0.0	.875	2.53
591.0	6532.8	6517.8	16590.2	-.008	11026.4	11463.3	0.0	0.0	0.0	.874	2.55
592.0	6549.7	6534.7	16894.9	-.003	11038.3	11494.6	0.0	0.0	0.0	.874	2.54
593.0	6566.6	6551.6	16968.5	-.002	11049.3	11506.1	0.0	0.0	0.0	.874	2.55
594.0	6583.6	6568.6	17003.7	-.000	11058.3	11517.5	0.0	0.0	0.0	.874	2.56
595.0	6600.6	6585.6	17019.7	-.004	11068.3	11529.0	0.0	0.0	0.0	.874	2.56
596.0	6617.8	6602.8	17187.5	.002	11078.6	11540.8	0.0	0.0	0.0	.874	2.55
597.0	6634.9	6619.9	17109.5	.009	11088.7	11552.4	0.0	0.0	0.0	.874	2.55
598.0	6651.9	6636.9	16954.0	-.010	11098.5	11563.5	0.0	0.0	0.0	.874	2.53
599.0	6668.9	6653.9	17052.2	.002	11108.4	11574.8	0.0	0.0	0.0	.874	2.57
[illegible]	[illegible]	[illegible]	16963.3	.007	11118.2	11585.9	0.0	0.0	0.0	.874	2.57

T	DKB	DDP	IV	K	VAV	VRMS	DT FOR X = 0.	0.	0.	ALPHA	DENS
			16609.4							.874	2.56
601.0	6702.7	6687.7		.005	11127.7	11596.5	0.0	0.0	0.0		
			16751.6							.874	2.54
602.0	6719.5	6704.5		.026	11137.0	11607.0	0.0	0.0	0.0		
			15902.0							.873	2.54
603.0	6735.4	6720.4		.047	11144.9	11615.4	0.0	0.0	0.0		
			14900.7							.872	2.47
604.0	6750.3	6735.3		-.076	11151.1	11621.6	0.0	0.0	0.0		
			16647.1							.866	2.58
605.0	6766.9	6751.9		-.020	11160.2	11631.7	0.0	0.0	0.0		
			17248.3							.866	2.59
606.0	6784.2	6769.2		-.004	11170.3	11643.2	0.0	0.0	0.0		
			17269.3							.866	2.60
607.0	6801.4	6786.4		.005	11180.3	11654.7	0.0	0.0	0.0		
			17266.9							.866	2.58
608.0	6818.7	6803.7		.036	11190.3	11666.2	0.0	0.0	0.0		
			16162.1							.865	2.57
609.0	6834.9	6819.9		.006	11198.5	11675.0	0.0	0.0	0.0		
			16251.5							.865	2.52
610.0	6851.1	6836.1		.002	11206.8	11684.0	0.0	0.0	0.0		
			16434.6							.865	2.48
611.0	6867.6	6852.6		-.024	11215.3	11693.3	0.0	0.0	0.0		
			17071.4							.864	2.51
612.0	6884.6	6869.6		-.010	11224.9	11704.1	0.0	0.0	0.0		
			17103.4							.864	2.55
613.0	6901.7	6886.7		.008	11234.5	11715.0	0.0	0.0	0.0		
			16861.4							.864	2.55
614.0	6918.6	6903.6		.034	11243.6	11725.2	0.0	0.0	0.0		
			16060.7							.863	2.50
615.0	6934.7	6919.7		-.000	11251.5	11733.5	0.0	0.0	0.0		
			16355.6							.863	2.46
616.0	6951.0	6936.0		-.011	11259.8	11742.5	0.0	0.0	0.0		
			16437.1							.863	2.50
617.0	6967.4	6952.4		.008	11269.1	11751.6	0.0	0.0	0.0		
			16519.5							.863	2.44
618.0	6984.0	6969.0		-.029	11276.6	11760.9	0.0	0.0	0.0		
			16921.3							.863	2.48
619.0	7000.9	6985.9		-.002	11285.8	11771.1	0.0	0.0	0.0		
			16887.6							.863	2.50
620.0	7017.8	7002.8		-.009	11294.8	11781.1	0.0	0.0	0.0		

T	DKB	DDP	IV	K	VAV	VRMS	DT FOR X = 0.	0.	0.	ALPHA	DENS
621.0	7034.9	7019.9	17093.8	.003	11304.1	11791.6	0.0	0.0	0.0	.863	2.51
622.0	7052.0	7037.0	17089.3	.008	11313.4	11802.0	0.0	0.0	0.0	.863	2.50
623.0	7068.8	7053.8	16833.6	-.011	11322.3	11811.8	0.0	0.0	0.0	.863	2.49
624.0	7085.8	7070.6	17032.9	-.003	11331.4	11822.0	0.0	0.0	0.0	.863	2.52
625.0	7103.1	7088.1	17282.7	.007	11341.0	11832.8	0.0	0.0	0.0	.863	2.50
626.0	7120.3	7105.3	17211.6	-.007	11350.3	11843.3	0.0	0.0	0.0	.863	2.48
627.0	7137.5	7122.5	17227.1	-.025	11359.7	11853.8	0.0	0.0	0.0	.862	2.51
628.0	7155.3	7140.3	17719.8	-.056	11369.0	11865.5	0.0	0.0	0.0	.862	2.56
629.0	7174.1	7159.1	18857.0	-.017	11361.8	11879.9	0.0	0.0	0.0	.859	2.69
630.0	7193.5	7178.5	19414.0	-.001	11394.5	11895.6	0.0	0.0	0.0	.859	2.71
631.0	7213.0	7198.0	19481.5	-.001	11407.3	11911.5	0.0	0.0	0.0	.859	2.70
632.0	7232.6	7217.6	19560.5	-.005	11420.2	11927.4	0.0	0.0	0.0	.859	2.70
633.0	7252.1	7237.1	19563.9	.008	11433.1	11943.4	0.0	0.0	0.0	.859	2.73
634.0	7271.7	7256.7	19517.7	.006	11445.8	11959.1	0.0	0.0	0.0	.859	2.69
635.0	7291.1	7276.1	19468.4	.001	11458.5	11974.6	0.0	0.0	0.0	.859	2.67
636.0	7310.4	7295.4	19276.4	.001	11470.8	11989.6	0.0	0.0	0.0	.859	2.68
637.0	7329.7	7314.7	19264.2	-.007	11483.0	12004.5	0.0	0.0	0.0	.859	2.68
638.0	7349.0	7334.0	19357.2	-.004	11495.3	12019.5	0.0	0.0	0.0	.859	2.71
639.0	7368.5	7353.5	19447.2	-.001	11507.8	12034.7	0.0	0.0	0.0	.859	2.72
640.0	7388.0	7373.0	19550.5	.001	11520.3	12050.1	0.0	0.0	0.0	.859	2.71

T	DKB	DDP	IV	K	VAV	VRMS	DT FOR X = 0.	0.	0.	ALPHA	DENS
			19552.6							.859	2.70
641.0	7407.6	7392.6		.003	11532.9	12065.4	0.0	0.0	0.0		
			19570.2							.859	2.68
642.0	7427.1	7412.1		.004	11545.4	12080.8	0.0	0.0	0.0		
			19566.8							.859	2.66
643.0	7446.7	7431.7		-.006	11557.9	12096.0	0.0	0.0	0.0		
			19520.2							.859	2.70
644.0	7466.2	7451.2		.006	11570.2	12111.1	0.0	0.0	0.0		
			19565.7							.859	2.67
645.0	7485.7	7470.7		-.006	11582.5	12126.0	0.0	0.0	0.0		
			19553.2							.859	2.70
646.0	7505.3	7490.3		-.000	11594.9	12141.0	0.0	0.0	0.0		
			19530.7							.859	2.70
647.0	7524.8	7509.8		.000	11607.1	12155.9	0.0	0.0	0.0		
			19530.4							.859	2.70
648.0	7544.4	7529.4		.001	11619.4	12170.7	0.0	0.0	0.0		
			19494.5							.859	2.70
649.0	7563.9	7549.0		.008	11631.5	12185.4	0.0	0.0	0.0		
			19208.3							.859	2.72
650.0	7583.1	7568.1		-.012	11643.2	12199.3	0.0	0.0	0.0		
			19487.9							.859	2.73
651.0	7602.5	7587.5		-.003	11655.2	12213.6	0.0	0.0	0.0		
			19578.5							.859	2.72
652.0	7622.1	7607.1		.005	11667.4	12228.5	0.0	0.0	0.0		
			19468.1							.858	2.64
653.0	7641.6	7626.6		.016	11679.3	12242.9	0.0	0.0	0.0		
			19375.2							.858	2.70
654.0	7661.0	7645.0		-.013	11691.1	12257.0	0.0	0.0	0.0		
			19432.4							.858	2.71
655.0	7680.4	7665.4		.001	11702.7	12271.2	0.0	0.0	0.0		
			19350.3							.858	2.73
656.0	7699.8	7684.8		-.005	11714.6	12285.1	0.0	0.0	0.0		
			19395.0							.858	2.70
657.0	7719.2	7704.2		.011	11726.3	12299.0	0.0	0.0	0.0		
			19202.2							.858	2.76
658.0	7738.4	7723.4		-.019	11737.6	12312.4	0.0	0.0	0.0		
			19523.4							.858	2.70
659.0	7757.9	7742.9		.015	11749.5	12326.5	0.0	0.0	0.0		
			19402.7								
660.0	7777.3	7762.3		-.005	11761.0	12340.4	0.0	0.0	0.0		

I	DKB	DDP	IV	K	VAV	VRMS	O.	DT FOR X O.	U.	ALPHA	DENS
661.0	7796.6	7781.8	19467.8	.015	11772.7	12354.3	0.0	0.0	0.0	.857	2.72
662.0	7815.9	7800.9	19185.2	-.005	11783.9	12367.4	0.0	0.0	0.0	.857	2.68
663.0	7835.3	7820.3	19330.5	-.007	11795.3	12380.9	0.0	0.0	0.0	.857	2.68
664.0	7854.7	7839.7	19433.5	.003	11806.8	12394.5	0.0	0.0	0.0	.857	2.70
665.0	7874.0	7859.0	19299.3	-.002	11818.1	12407.8	0.0	0.0	0.0	.857	2.70
666.0	7893.4	7878.4	19373.3	.003	11829.4	12421.2	0.0	0.0	0.0	.857	2.70
667.0	7912.6	7897.6	19237.3	.005	11840.5	12434.2	0.0	0.0	0.0	.857	2.70
668.0	7931.7	7916.7	19120.9	.030	11851.4	12446.9	0.0	0.0	0.0	.857	2.70
669.0	7950.1	7935.1	18383.8	-.030	11861.2	12457.9	0.0	0.0	0.0	.856	2.64
670.0	7969.1	7954.1	19014.9	-.003	11871.8	12470.2	0.0	0.0	0.0	.856	2.71
671.0	7988.6	7973.6	19485.5	.012	11883.2	12483.6	0.0	0.0	0.0	.856	2.66
672.0	8008.0	7993.0	19382.8	-.009	11894.4	12496.7	0.0	0.0	0.0	.856	2.61
673.0	8027.4	8012.4	19427.3	-.011	11905.5	12509.9	0.0	0.0	0.0	.855	2.65
674.0	8047.0	8032.0	19572.3	-.004	11916.9	12523.3	0.0	0.0	0.0	.855	2.69
675.0	8066.6	8051.6	19593.2	.001	11928.3	12536.7	0.0	0.0	0.0	.855	2.71
676.0	8086.2	8071.2	19588.4	.004	11939.6	12550.1	0.0	0.0	0.0	.855	2.71
677.0	8105.6	8090.6	19409.3	.006	11950.7	12563.0	0.0	0.0	0.0	.855	2.71
678.0	8124.7	8109.7	19148.6	-.011	11961.3	12575.2	0.0	0.0	0.0	.855	2.71
679.0	8144.2	8129.2	19406.8	.003	11972.2	12588.0	0.0	0.0	0.0	.855	2.73
680.0	8163.6	[illegible]	19459.1	-.001	11983.3	12600.9	0.0	0.0	0.0	.855	2.71

T	DKB	DOP	IV	K	VAV	VRMS	DT FOR X = U.	0.	Q.	ALPHA	DENS
			19524.1							.855	2.70
681.0	8183.1	8168.1		.005	11494.3	12613.8	0.0	0.0	0.0		
			19450.1							.855	2.69
682.0	8202.6	8187.6		-.003	12005.3	12626.5	0.0	0.0	0.0		
			19447.9							.855	2.70
683.0	8222.0	8207.0		-.004	12016.2	12639.2	0.0	0.0	0.0		
			19454.5							.855	2.72
684.0	8241.5	8226.5		.003	12027.0	12651.9	0.0	0.0	0.0		
			19447.0							.855	2.71
685.0	8260.9	8245.9		.004	12037.9	12664.4	0.0	0.0	0.0		
			19412.0							.855	2.69
686.0	8280.3	8265.3		.001	12048.6	12676.9	0.0	0.0	0.0		
			19318.4							.855	2.70
687.0	8299.7	8284.7		0.000	12059.2	12689.1	0.0	0.0	0.0		
			19318.4							.855	2.72
688.0	8319.0	8304.0		0.000	12069.7	12701.2	0.0	0.0	0.0		

END OF COMPUTATION

REISSUE

STATE: ARIZONA
COUNTY: PIMA
API 02-019-20015

WELL CLASS: S
OPR: PHILLIPS PET

17S-15E 10
SE SW NE
2630 FNL 1860 FEL
STATUS: D&A

A-1 MOUNTAIN VIEW STATE

SPUD: 06/06/82 COMP: 07/22/82 ELEV: 3141 GR
TD: 8333 (07/21/82) FM/TD: UNKNOWN
CONTR: BRINKERHOFF DRLG RIG #9 (R)
PROJ DEPTH/FM: 9000 PERMIT #796

COMP 7/22/82, D&A ONE CORE, 14 SDWL CORES, NO DSTS FIRST REPORT & COMPLETION REISSUE TO ADD & CORRECT DATA REPLACES CARD ISSUED 3/23/83

LOC DESCRIPTION: 14 MI SE OF TUCSON, AZ; LAT: 3197088 LONG: 11079743; ARIZONA DRY HOLE;
CASING: 9 5/8 @ 1071 W/913 SX;
LOG TYPES: BHCS, CAL, DILL, GRL, SP; BHC 0-1082, 1071-8315, CNL 1071-8327, DIPM 1071-8315, DISF 1071-8315, FDC 1071-8327, MUD 1071-8315, SONL 0-1082, 1071-8315;

CORE # 1 8325-8333 REC: 7 FT NO DESCRIPTION AVAILABLE FM NOT RPTD;
SDWL CORES: TOOK 14 SDWL CORES, 5630-7170, FM NOT RPTD;
OPER ADD: PO BOX 2920, CASPER, WY, 82602

COPYRIGHT 1997 PETROLEUM INFORMATION/DWIGHTS LLC

DATE 12/08/97CARD #00001-F COR

M-24.

ARIZONA
PIMA CO
WILDCAT (S)

Petroleum Information
CORPORATION
A Subsidiary of A.C. Nielsen Company

Twp 17s-15e Status 796
Section 10 D&A
sw ne
2630 fnl 1860 fel

OPR: Phillips Pet WELL: A-1 Mountain View-State

Spud: 6/6/82 Comp: 7/22/82 Elev: 3141 Gr TD: 8333/(7/21/82)
Contr: Brinkerhoff #9
Casing: 9 5/8 @ 1071 w/913
Log Types: DILL/GRL/CAL/SP/BHCS
Log Tops: Not reported
Cores: Core #1, 8325-33, rec 7, no details. Cut 14 sdwl cores 5630-7170, rec 14, no further details.
DST'S: No tests
IP: D&A

PI Base Map Arizona Dry Hole API 02-019-20015 AZ15-S1-0984

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FORM NO. 327

796

OFFICE OF
Oil and Gas Conservation Commission
STATE OF ARIZONA
1645 WEST JEFFERSON, SUITE 420
PHOENIX, ARIZONA 85007
PHONE: (602) 255-5161

April 10, 1984

Mr. David Rhode
Shell Oil Company
P. O. Box 831
Houston, Texas 77001

Dear David:

Per your telephone request to Mr. Rudy Ybarra on April 5, 1984, enclosed you will find logs on the following Phillips Petroleum wells:

Arizona State A-1, Sec. 2, T.7S, R.10E
Douglas A-1 State, Sec. 14, T.23S, R.29E
Huachuca A-1 State, Sec. 16, T.20S, R.20E
Mountain View A-1 State, Sec. 10, T.17S, R.15E
Redondo A-1 State, Sec. 36, T.17S, R.8E

At the present time, we do not have duplicate logs on the Phillips Tombstone State 1-A, Sec. 14, T.20S, R.23E. I have requested duplicate logs from Phillips and we should be receiving them shortly. However, Rocky Mountain Well Log Service has requested them as soon as they are received. As soon as they return them, I will send them to you.

Would you please sign the attached list of logs as acknowledgement of receipt and return the copy to me. A letter will follow with a bill for the postage.

If I can be of any further assistance, please let me know.

Sincerely,

Sheila

Sheila Burgan
Secretary
Enforcement Section

Enclosures
Attachment - 2

PHILLIPS PETROLEUM COMPANY LOG

Arizona State A-1
Sec. 2, T.7S, R.10E
Pinal County, Arizona P/N 702

1 each Mud Log, 03/06/80

Douglas A-1 State
Sec. 14, T.23S, R.29E
Cochise County, Arizona P/N 793

1 each Mud Log, 04/18/82

1 each BCSL, Dual Induction, #1, 04/22/82

1 each BCSL, CFDN, Dual Induction, Directional Survey, Dipmeter, Directional, Calibrated Velocity Log, Arrow Plot from Cluster Program, #2, 06/21/82

Huachuca A-1 State
Sec. 16, T.20S, R.20E
Cochise County, Arizona P/N 794

1 each Mud Log, 03/26/82

1 each Dual Induction, BCSL, #1, 03/27/82

1 each Dual Induction, BCSL, #2, 05/31/82

1 each Dipmeter, Directional Log, CNFS, #2, 06/01/82

1 each Seismic Velocity Survey & Velocity Log Calibration

Mountain View A-1 State
Sec. 10, T.17S, R.15E
Pima County, Arizona P/N 796

1 each Mud Log, 06/06/82

1 each Dual Induction, #1, 05/08/82; BCSL, #1, 06/08/82

1 each Dipmeter, BCSL, Dual Induction, #2, 07/19/82; CNFD, Sidewall Core Samples, #2, 07/21/82

1 each Velocity Survey W/Calculation of Synthetic Seismogram

Redondo A-1 State
Sec. 36, T.17S, R.8E
Pima County, Arizona P/N 797

1 each Mud Log, 02/11/82

1 each Dual Induction, BCSL, #1, 02/13/82; CNFD, #1, 03/19/82

1 each Dual Induction, Dipmeter, #2, 03/19/82; BCSL, #2, 03/18/82

1 each Seismic Velocity Survey & Velocity Log Calibration

RECEIVED BY:_____ DATE_____

RECEIVED
JUL 27 1983
O & G CONS. COMM.

PHILLIPS PETROLEUM COMPANY
DENVER, COLORADO 80237
8055 EAST TUFTS AVENUE PARKWAY

DATA TRANSMITTAL

DATE: 25 July 1983

TO: OIL AND GAS CONSERVATION COMMISSION
1645 W. Jefferson, Suite 420
Phoenix, Arizona 85007
Attn: A. K. Doss

RE: WELL NAME PHILLIPS PETROLEUM MOUNTAIN VIEW STATE A #1
Sec. 10-17S 15E
Pima County, Arizona

Mailed 7-29-3

ENCLOSED PLEASE FIND THE FOLLOWING:

1. ____ copies of Approved Well Permit
2. ____ copies of Core Analysis/Description
3. ____ copies of Drilling History
4. ____ copies of DST Charts/Reports
5. ____ copies of Fluid (gas, water, oil) Analysis
6. ____ copies of Geological Prognosis and Drilling Program
7. ____ copies of Geological Report
8. ____ copies of Survey Plat
9. ____ copies of Well Completion Report
10. ____ copies of Well Permit Application
11. ____ copies of Field Prints of Logs
12. 2 copies of Final Prints of Logs Mudlog 47' to T.D. 8333'
    2 copies of Velocity Survey w/ Calculation of Synthetic Seismogram
    ____ copies of
    ____ copies of
    ____ copies of

RECEIVED BY: [signature] DATE: 7-27-83

PLEASE ACKNOWLEDGE RECEIPT BY SIGNING AND RETURNING THE ENCLOSED COPY TO THE ABOVE ADDRESS. THANK YOU.

Pat Bertuzzi
Pat Bertuzzi - Development - 7th Floor

PHILLIPS PETROLEUM COMPANY
DENVER, COLORADO 80237
8055 EAST TUFTS AVENUE PARKWAY

DATA TRANSMITTAL

TO: OIL AND GAS CONSERVATION COMMISSION
1645 W. Jefferson, Suite 420
Phoenix, Arizona 85007

DATE: 30 June 1983

Attn: Mr. A. K. Doss

RE: WELL NAME Phillips-Mountain View State A#1
Sec 10-17S 15E
Pima County, Arizona

ENCLOSED PLEASE FIND THE FOLLOWING:

1. ____ copies of Approved Well Permit
2. ____ copies of Core Analysis/Description
3. ____ copies of Drilling History
4. ____ copies of DST Charts/Reports
5. ____ copies of Fluid (gas, water, oil) Analysis
6. ____ copies of Geological Prognosis and Drilling Program
7. ____ copies of Geological Report
8. ____ copies of Survey Plat
9. ____ copies of Well Completion Report
10. ____ copies of Well Permit Application
11. 2 copies of Field Prints of Logs Sidewall Core Samples Run#2 7-21-82
12. 2 copies of ~~Final~~ Field Prints of Logs Continious Dipmeter Run #2 7-19-82
    2 copies of Field: Compensated Neutron Formation Run#2 7-21-82
    2ea copies of Field: Borehole Comp. Sonic log Runs#1+#2 6-8-82/7-19-82
    2ea copies of Field: Dual Induction-SFL Runs #1+#2 5-8-82/7-19-82
    ____ copies of ____

RECEIVED BY: ____ DATE: ____

PLEASE ACKNOWLEDGE RECEIPT BY SIGNING AND RETURNING THE ENCLOSED COPY TO THE ABOVE ADDRESS. THANK YOU.

Pat Bertuzzi

Pat Bertuzzi - Development - 7th Floor

PHILLIPS PETROLEUM COMPANY
DENVER, COLORADO 80237
8055 EAST TUFTS AVENUE PARKWAY

July 28, 1982

A.K. Doss
Arizona Oil and Gas
Conservation Commission
1645 West Jefferson, Suite 4200
Phoenix, Arizona 85007

Dear Mr. Doss:

With this letter we are sending core chips taken at one foot intervals from cores cut on our current drilling program since our last shipment on June 10. The samples included in this shipment are:

S/N 1833
P/N 793

Douglas State A-1
NW NW 14-23S-29E, Cochise County
Core 3 - 7027'-7054'

7027-7046
7048-7054

S/N 1840
P/N 796

Mountain View State A-1
SW NE 10-17S-15E, Pima County
Core 1 - 8325'-8352'

8325-27
32
5329-

S/N 1839
P/N 795

Kirkland State A-1
SE SE 32-14N-6W, Yavapai County
Core 1 - 1118'-1127'

Any questions regarding these samples or the drilling project should be directed to me at (303) 779-8989, extension 475. Please note our new mailing address.

Sincerely,

Jamie Robinson
Geologist

cc: C.W. Betton
(r) file

JR/bm

February 2, 1982

Mr. D. J. Fisher
Phillips Petroleum Co.
P.O. Box 2920
Casper, Wyoming 82602

Dear Mr. Fisher:

Enclosed are approved application for permit to drill, permit to drill, and receipt for the following six strat wells:

Permit No.	
793	Douglas Al State
794	Huachaca Al State
795	Kirkland Al State
796	Mtn View Al State
797	Redondo Al State
798	Safford Al State

As requested, this Commission has approved a one-year extension of the drilling permits issued February 1, 1982, on the above wells.

If we can be of further service, please advise.

Sincerely,

A. K. Doss
Executive Director

/os
Enc.

RECEIVED AKD

1982

O & G CONS. COMM.

PHILLIPS PETROLEUM COMPANY
P. O. Box 2920
Casper, WY 82602-2920

January 27, 1982

Mr. A. K. Doss
Oil & Gas Conservation Commission
State of Arizona
1645 West Jefferson
Suite 420
Phoenix, AZ 85007

Re: Applications For Permit
To Drill Various Counties,
Arizona.

Dear Sir:

Enclosed are APD's to drill the following six "strat" wells:

Douglas State "A" No. 1
Huachaca State "A" No. 1
Kirkland State "A" No. 1
796 Mtn. View State "A" No. 1
Redondo State "A" No. 1
Safford State "A" No. 1

As approved by you in a telephone conversation with Frank Lyte, of this office, on January 25th, the certified plats are being prepared by the surveyor and will be mailed to you as soon as received in this office. As previously done by the A.O. & G.C., granting a one year extension to these six permits is respectfully requested.

Your continued cooperation in expediting approvals by your office and other Arizona State agencies will be appreciated.

Very truly yours,

PHILLIPS PETROLEUM COMPANY

D. J. Fisher
Area Manager

FGL/jj

Enclosure